

# Modeling Fire Plume Rise in AIRPACT5 - a preliminary study

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2017 NW-Airquest Annual Meeting

6/14/2017 – 6/16/2017

\*\*\* Preliminary study, please do not cite \*\*\*

# Difficulty in Fire Modeling

- Fire Emission
  - Fuel loading
  - Consume
- Fire plume rise
- Lack of Observation data

## Smoke injection heights from fires in North America: analysis of 5 years of satellite observations

M. Val Martin<sup>1</sup>, J. A. Logan<sup>1</sup>, R. A. Kahn<sup>2</sup>, F.-Y. Leung<sup>3</sup>, D. L. Nelson<sup>4</sup>, and D. J. Diner<sup>5</sup>

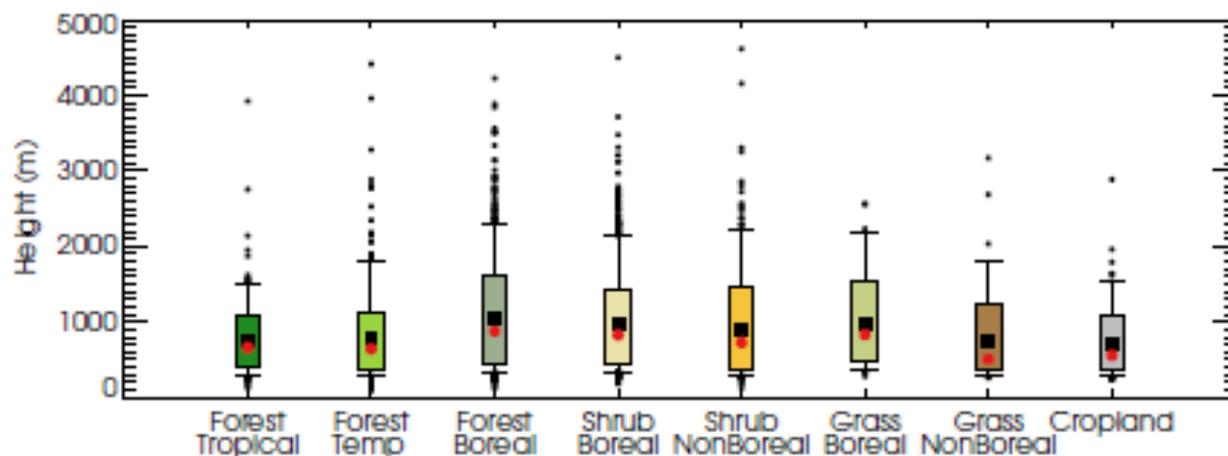
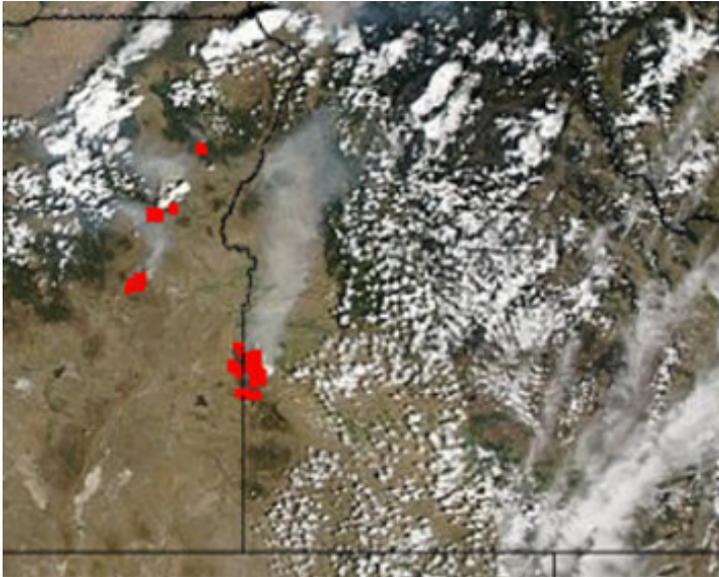
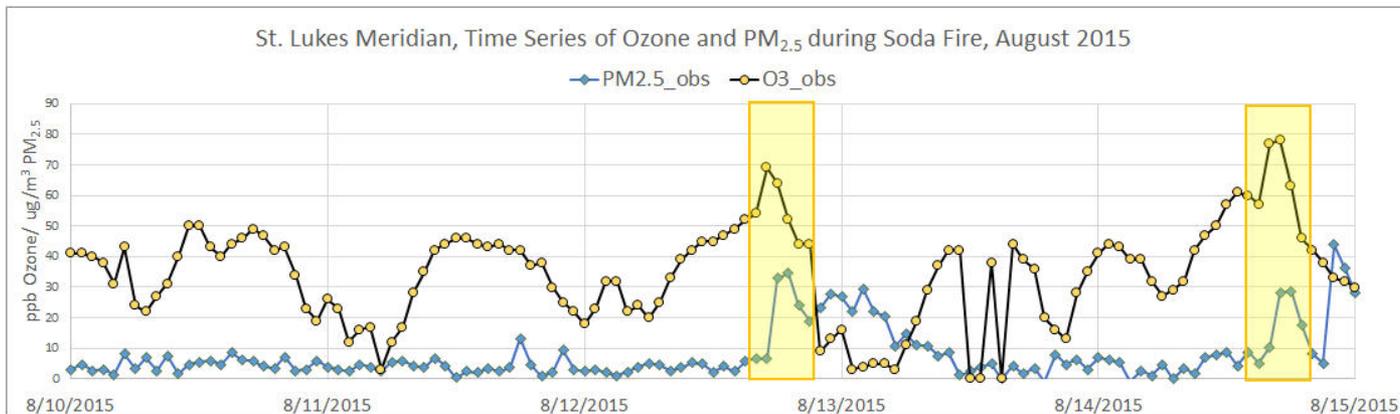


Fig. 6. Distribution of the median height above the terrain for smoke plumes in each biome (see Figure 3 for spatial distribution of the biomes). Bar plots indicate the distribution of the data. The medians (red circles) and the means (black squares) are shown along with the central 67% (color coded box) and the central 95% (thin black lines). Data that fall outside the bar plots are plotted with black circles.

# Soda Fire



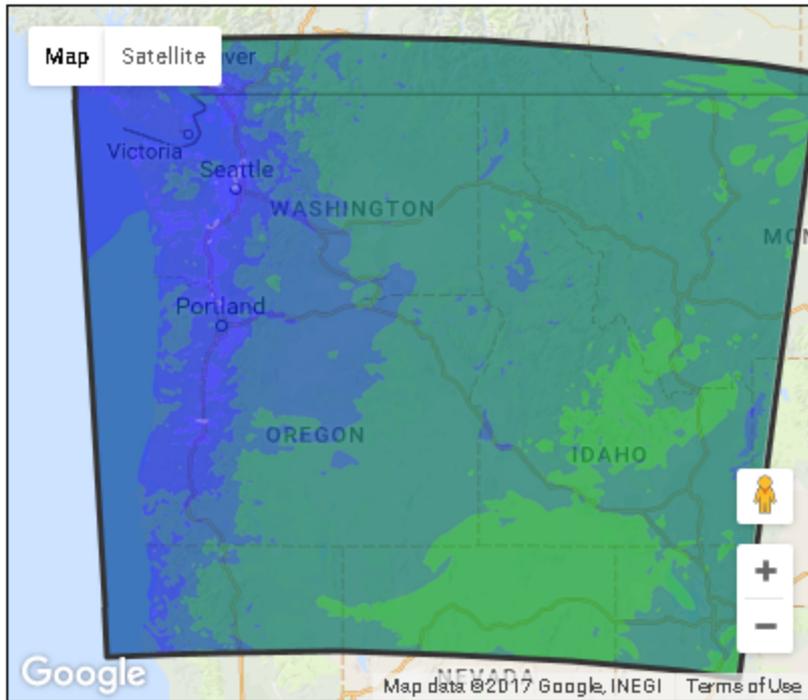
- 8/10/2015 – 8/15/2015
- PM<sub>2.5</sub> & Ozone data at St. Luke's (Meridian) and PM<sub>2.5</sub> data at Nampa
- No impact from other fires before 8/14/2015



# Soda Fire, Aug. 12 Flyover



# Modeling Setup

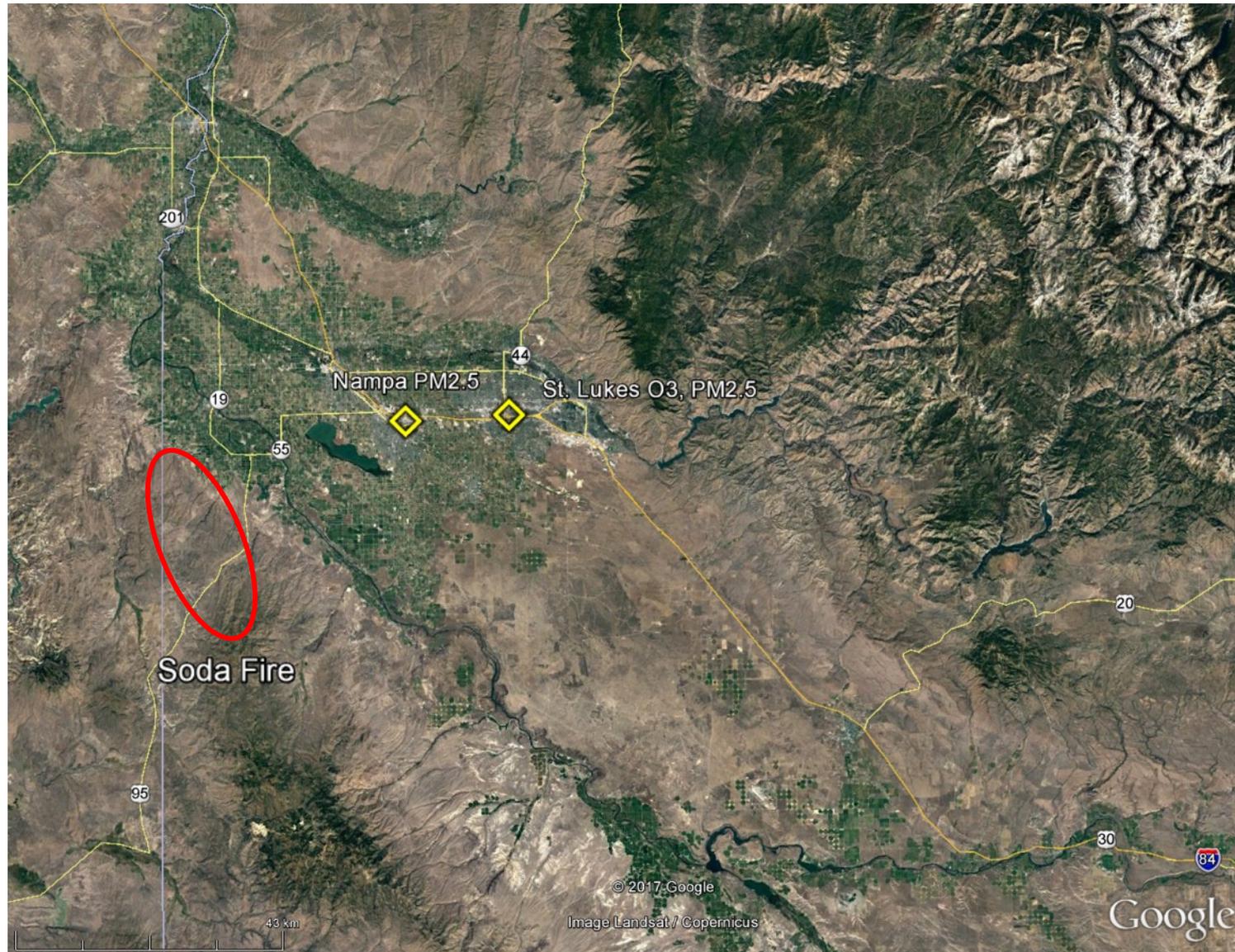


- The latest AIRPACT5 System (4km resolution)
- Updated onroad emission
- Soda fire emission generated from Bluesky Framework
- Plume rise determined in SMOKE

# Vertical Structure at St Lukes

Layer	Middle Height (m)
1	21.25
2	63.83
3	110.40
4	165.20
5	225.10
6	290.90
7	367.90
8	458.20
9	564.60
10	689.40
11	835.40
12	1007.00
13	1207.00
14	1759.00
15	2913.00
16	4709.00
17	7273.00
18	10280.00
19	13200.00
20	15990.00
21	18720.00

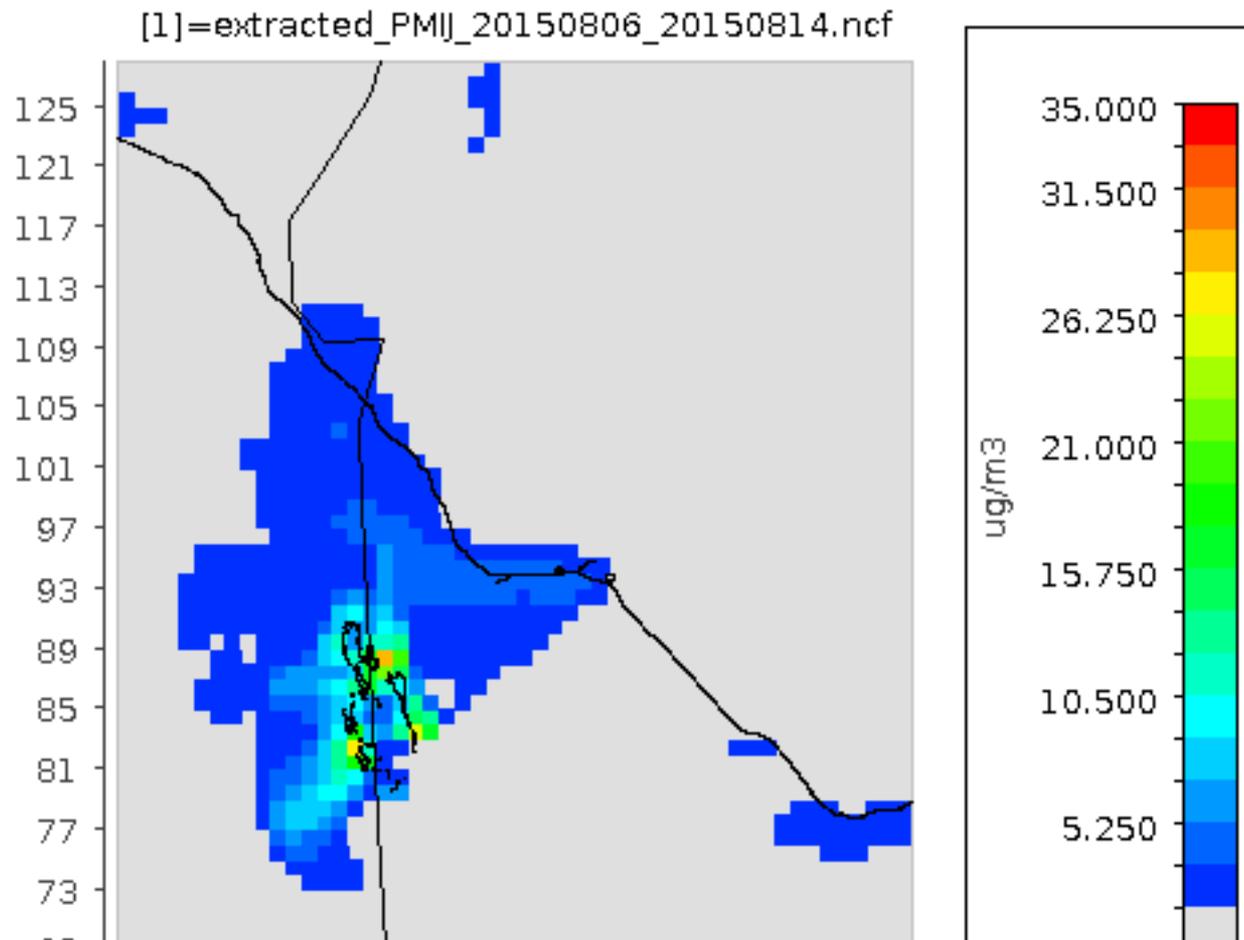
# Locations of Monitoring Sites



# Initial Model Performance (1)

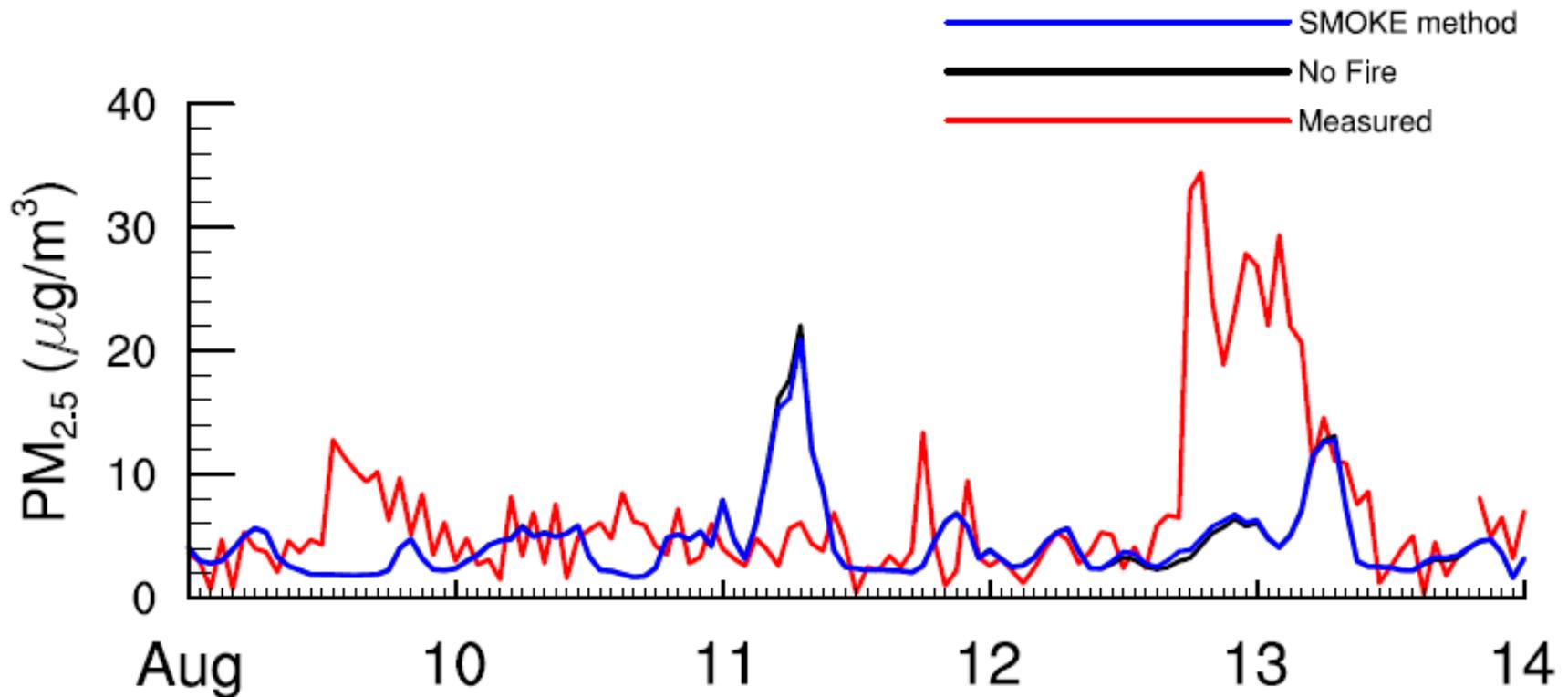
## Spatial

### Layer 1 PMIJ[1]



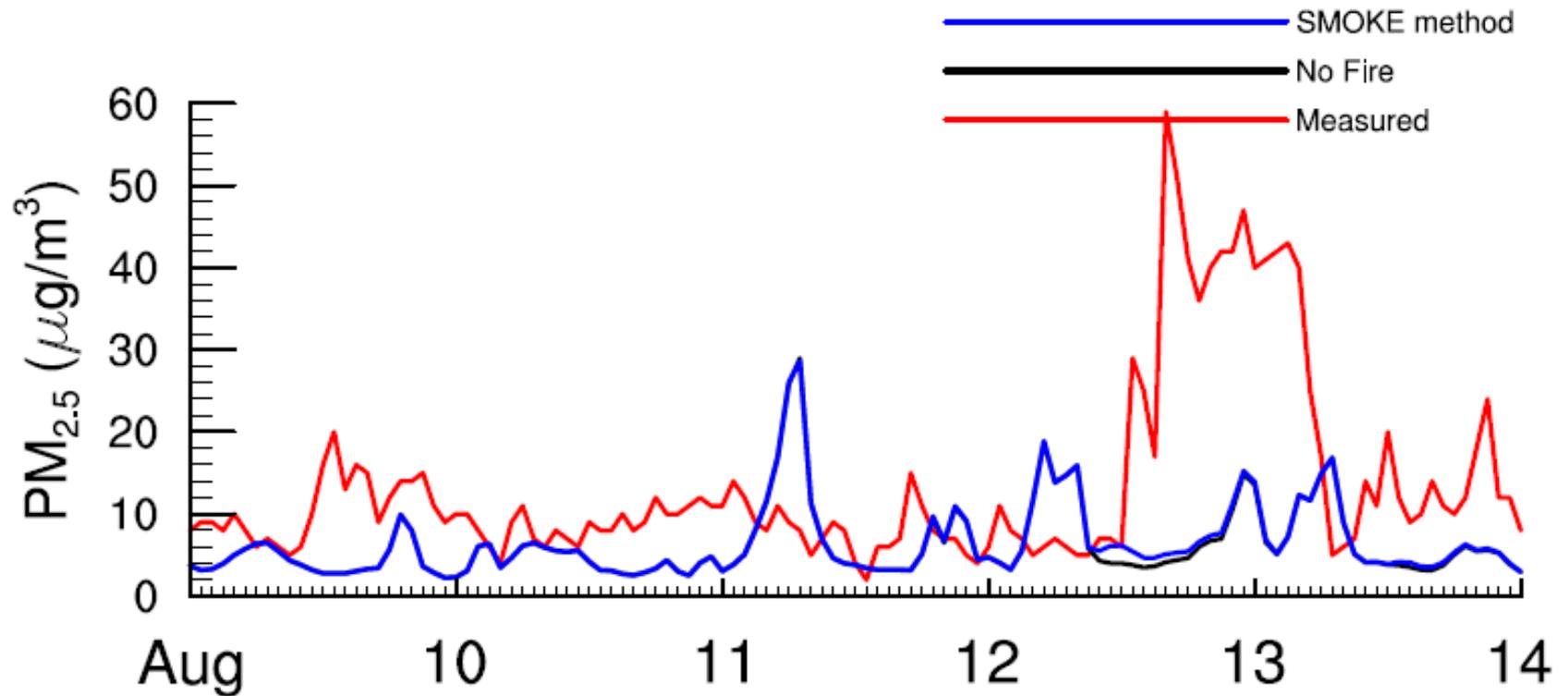
# Initial Model Performance (2)

## Time Series at St lukes



# Initial Model Performance (3)

## Time Series at Nampa



# Why???

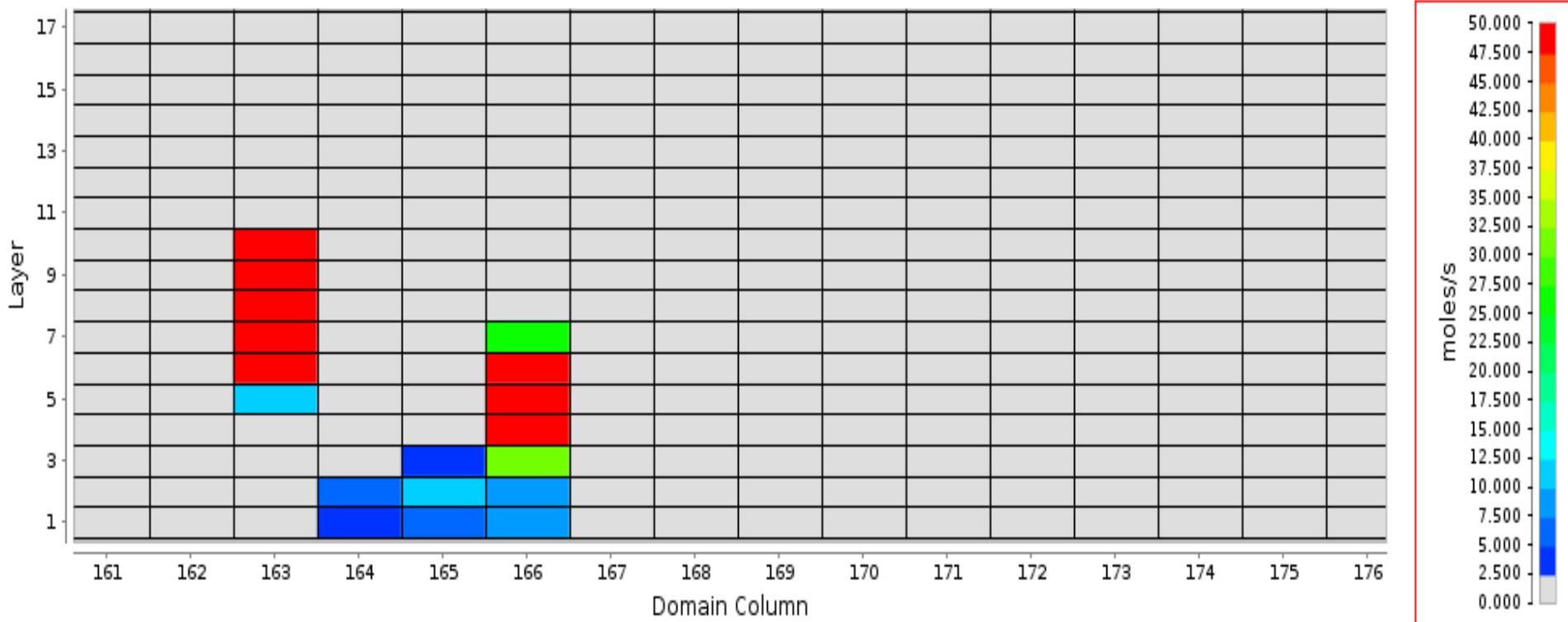
- Meteorology performance???
  - Evaluated the Meteorology performance
  - Checked neighboring grid cells to account wind direction uncertainty
- Emission???
  - STI data set under EPA contract
  - Best available
- Plume rise???

# Initial Model

## Emission Vertical Distribution

Row 86 CO[2]

[2]=pgts3d |\_2015224\_1\_AIRPACT\_04km\_fire.ncf



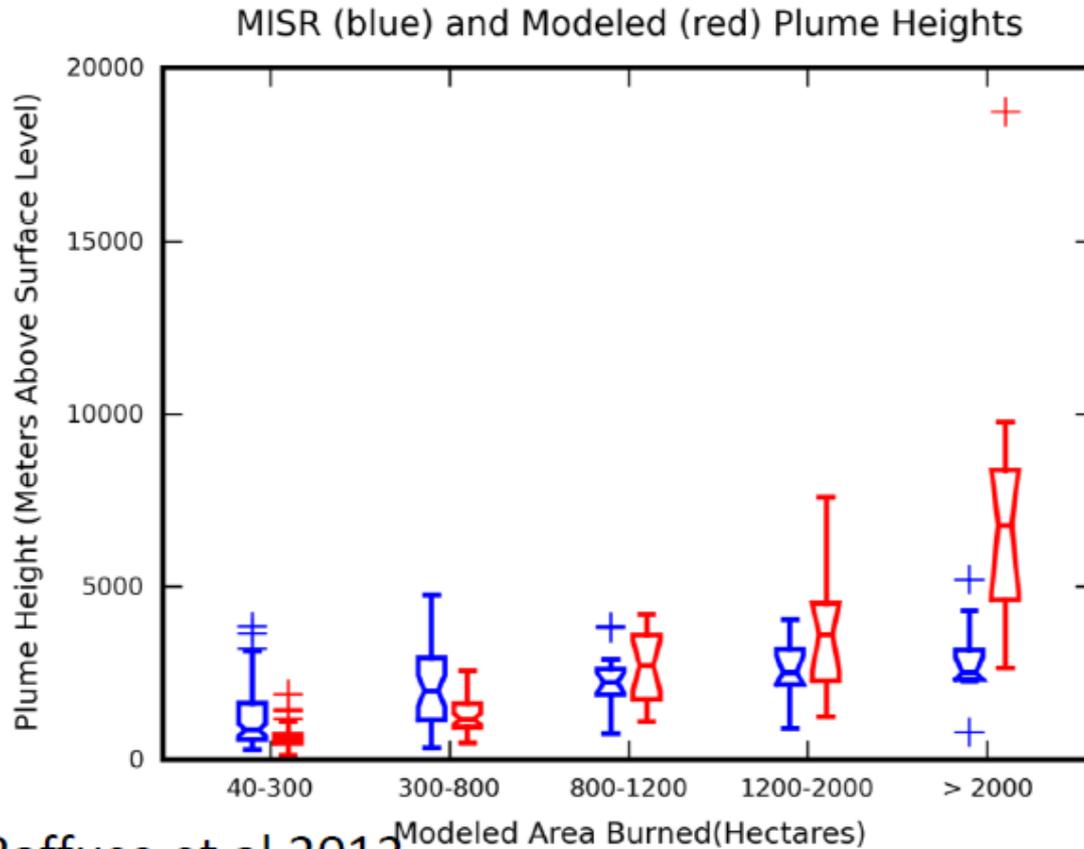
August 12, 2015 08:00:00 UTC

Min = 0, Max = 207.434

# Problems

- Smoldering fraction is too low
- Plume rise is too high

# Literature : Observation vs. Model



Raffuse et al 2012

# Plume Rise in SMOKE

*To be presented: 14th Internat. Emission Inventory Conf. "Transforming Emission Inventories Meeting Future Challenges Today" 4/11 -4/14/05 Las Vegas*

## **Wildfire Emission Modeling: Integrating BlueSky and SMOKE**

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Pacific Wildland Fire Sciences Laboratory  
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Seattle, WA 98103  
[oneill@fs.fed.us](mailto:oneill@fs.fed.us)

# Plume Rise in SMOKE (1)

1. Calculate Plume bottom and Plume top
  - Briggs plume rise algorithm
2. Determine smoldering fraction
3. Inject smoldering portion of emission between ground level to plume bottom
4. Inject flame portion of emission between plume bottom and plume top

# Plume Rise in SMOKE (2)

- Key inputs
  - Meteorology condition (wind speed, temperature, pressure, etc.)
  - Heat flux (BTU/hour)
    - [heat per acre] \* [acreage burned]
  - Acreage burned (acres/hour)
- Heat flux and acreage burned used in different steps, no connection in the model

# Plume Rise in SMOKE (3)

Calculate Plume bottom and Plume top

- Meteorology condition
- Buoyancy Flux

$$F = Q * 0.00000258$$

(1)

where  $F$  = buoyancy flux ( $\text{m}^4/\text{s}^3$ )  
 $Q$  = heat flux (BTU/hr)

**No acreage burned in equation???**

“1,000,000 British Thermal Units (BTUs) released over 100,000 acres is not equivalent, in terms of plume rise, to the same amount of heat released over 10,000 acres”  
(From DEASCO3 Report)

# Plume Rise in SMOKE (4)

Determine smoldering fraction

$$BE_{size} = 0.0703 * \ln(acres) + 0.3$$

(2)

where  $BE_{size}$  = buoyant efficiency  
 $acres$  = fire size in acres

The smoldering fraction ( $S_{fract}$ ) was calculated from the Bouyant efficiency as follows:

$$S_{fract} = 1 - BE_{size}.$$

# DEASCO3

## Objective

Quantify the contributions from fires to ambient levels of ozone using tools and procedures that are similar to those that will be used by state and local air agencies in State Implementation Plan (SIP) development.

## Deterministic and Empirical Assessment of Smoke's Contribution to Ozone (DEASCO<sub>3</sub>)

### Final Report

### Joint Fire Sciences Program Project # 11-1-6-6

Principal Investigator: Charles T. (Tom) Moore, Jr.

Western Governors' Association, Western Regional Air Partnership (WRAP)<sup>1</sup>

1600 Broadway, Suite 1700, Denver, CO 80202



#### Collaborators:

Air Sciences, Inc. – David Randall, Matthew Mavko, and colleagues

ENVIRON International Corp. – Ralph Morris, Bonyoung Koo, and colleagues

U.S. National Park Service – Mark Fitch, Michael George, Michael Barna, John Vimont

U.S. Forest Service – Bret Anderson, Ann Acheson



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1 - now with the Western States Air Resources Council (WESTAR), [tmoore@westar.org](mailto:tmoore@westar.org)

# WRAP/DEASCO3 (1)

## Fire Plume Classes

**Equation 1. FPCI Calculation Used to Determine Plume Height Bins**

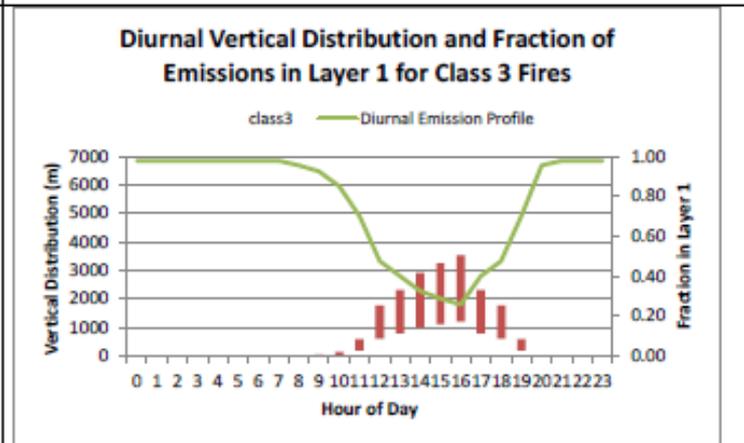
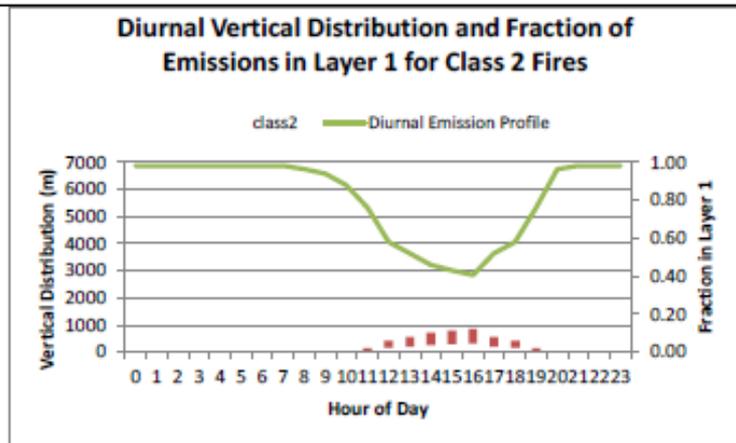
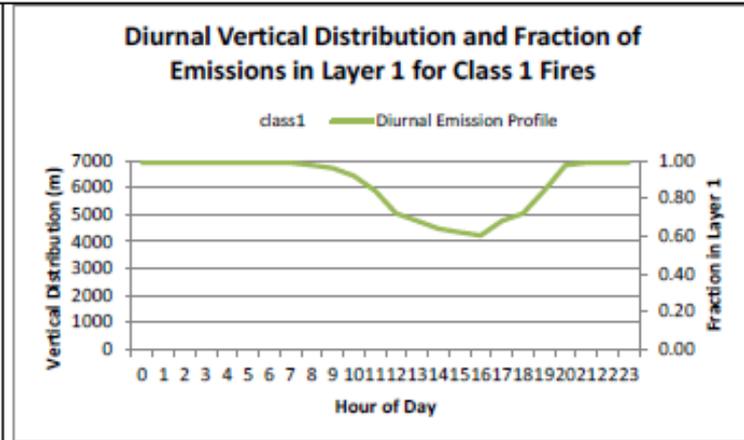
$$FPCI = \frac{\text{Flaming Phase Consumption}}{\sqrt{\text{acres}}}$$

**Table 1. Plume Height Bins Calculated Using FPCI and Fire Activity in the WRAP Region**

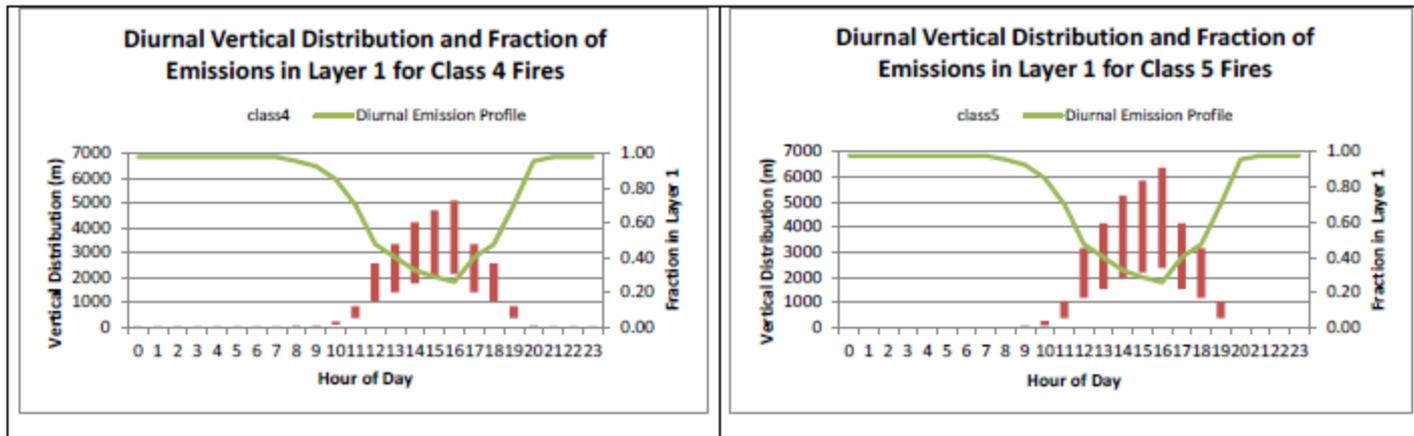
Plume Class	1	2	3	4	5	Total
<i>FPCI</i>	<i>0-75</i>	<i>75-300</i>	<i>300-675</i>	<i>675-1,250</i>	<i>&gt;1,250</i>	
Fire Days, DEASCO <sub>3</sub> 2008	48,725	9,912	1,167	366	96	60,266
Bin Frequency, DEASCO <sub>3</sub> 2008	81%	17%	1.9%	0.61%	0.16%	
Bin Frequency, WRAP 2002	62%	33%	4.5%	0.2%	0.02%	

# WRAP/DEASCO3 (2)

Class	Virtual Acreage
1	< 10
2	10 – 100
3	100 – 1000
4	1000 – 5000
5	>= 5000



# WRAP/DEASCO3 (3)



# Preserving smoldering fraction in SMOKE Processing

- Pre-determine the smoldering fraction
  - Literature (WRAP/DEASCO3)
- Virtual area concept
  - [Virtual area] =  $\text{EXP}((1 - 0.3 - [S\_fract])/0.0703)$
  - Different from WRAP virtual area

# Virtual Heat Approach (1)

- Inspired by DEASCO3 Flaming Phase Consumption Index
- Function of flaming phase heat and area burned
- Different fire (heat) density will have different plume rise
- Another way to think of it: multiple virtual flame fronts

1 acres

1001 acres



# Virtual Heat Approach (2)

## Definition:

- VH : Virtual Heat
- FPH : Flame Phase Heat (maximum heat)
- AR : Area burned

**If AR ≤ 1 acre :**

$$\mathbf{VH = FPH}$$

**If AR > 1 and < 1001 acres :**

$$\mathbf{VH = \frac{FPH}{\sqrt{AR}} + \left( FPH - \frac{FPH}{\sqrt{AR}} \right) * \left( \frac{1001 - AR}{1000} \right)}$$

**If AR ≥ 1001 acres :**

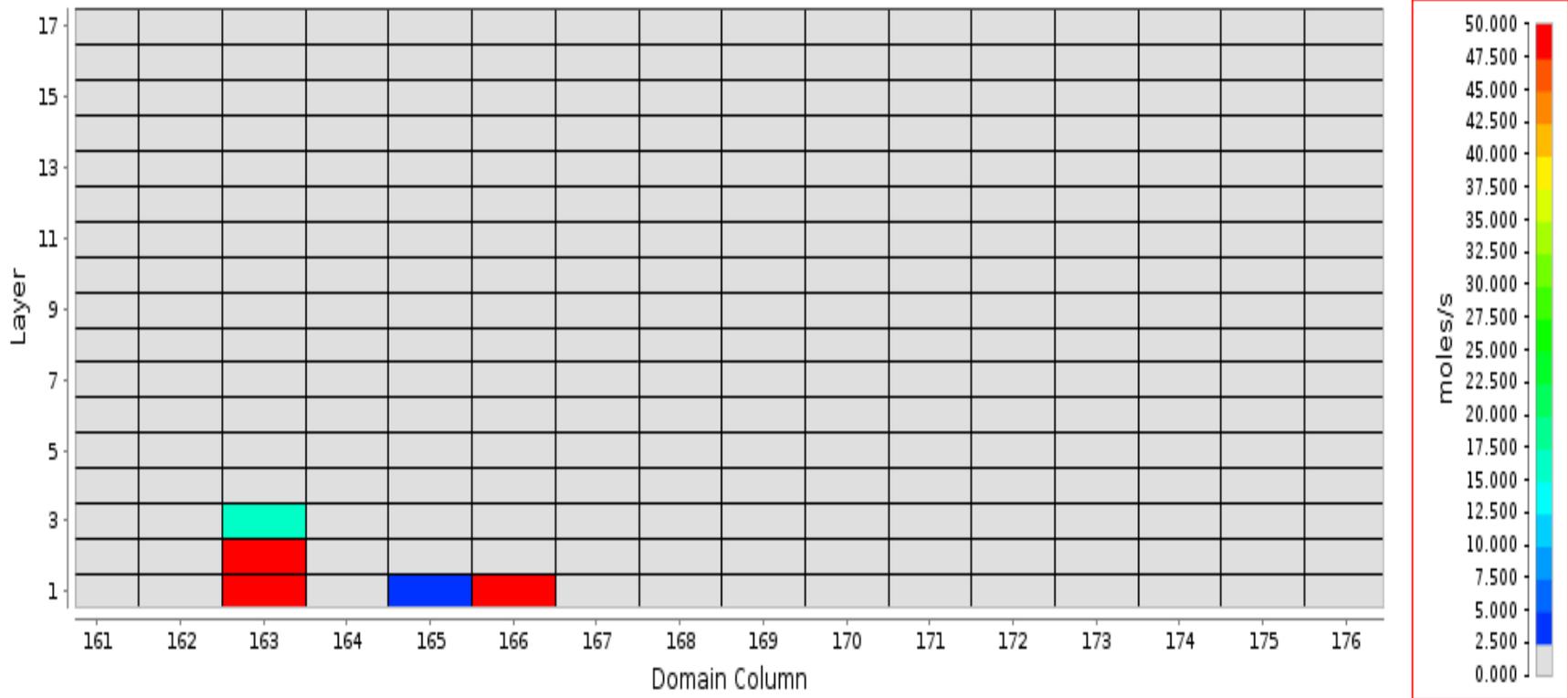
$$\mathbf{VH = \frac{FPH}{\sqrt{AR}}}$$

# New Method Result (1)

## Emission Vertical Distribution

Row 86 CO[4]

[4]=pgts3d |\_2015224\_1\_AIRPACT\_04km\_fire.ncf



August 12, 2015 08:00:00 UTC

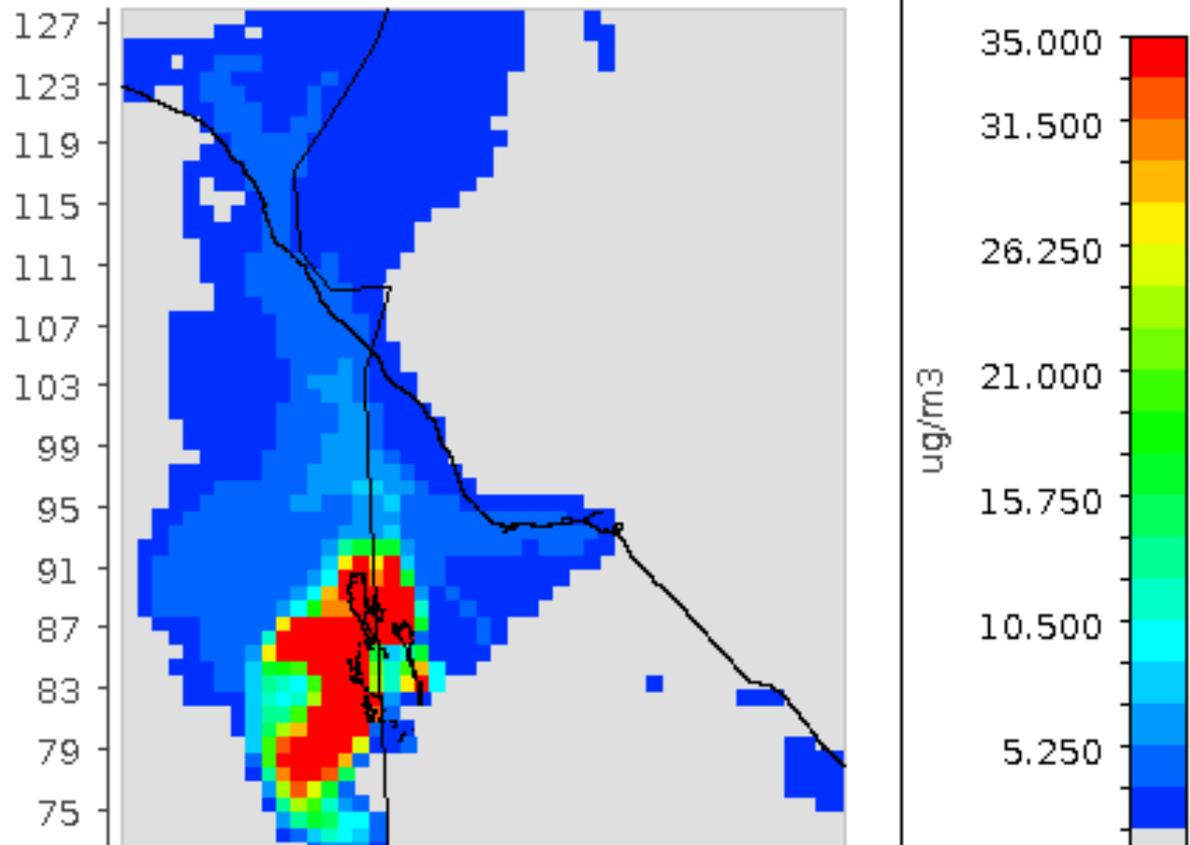
Min = 0, Max = 114.529

# New Method Result (2)

## Spatial

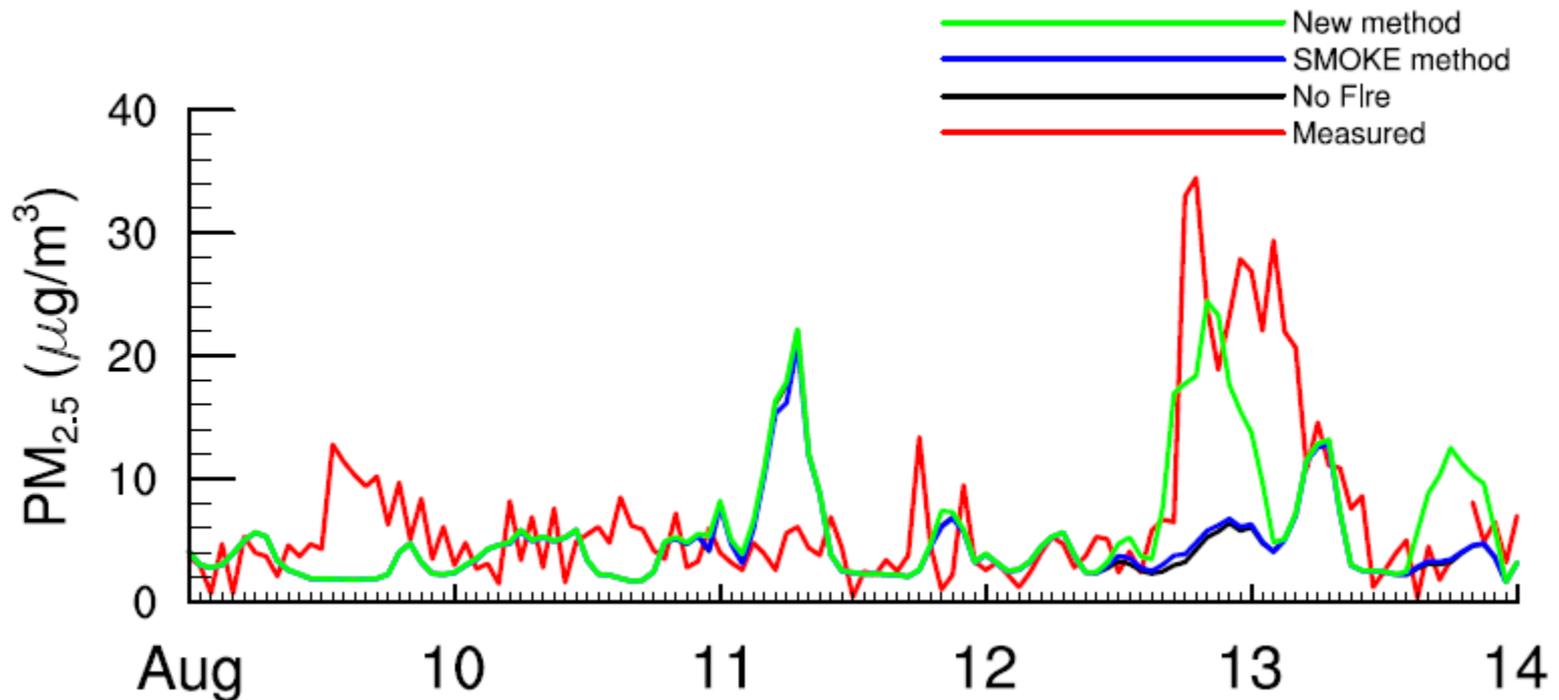
### Layer 1 PM10[3]

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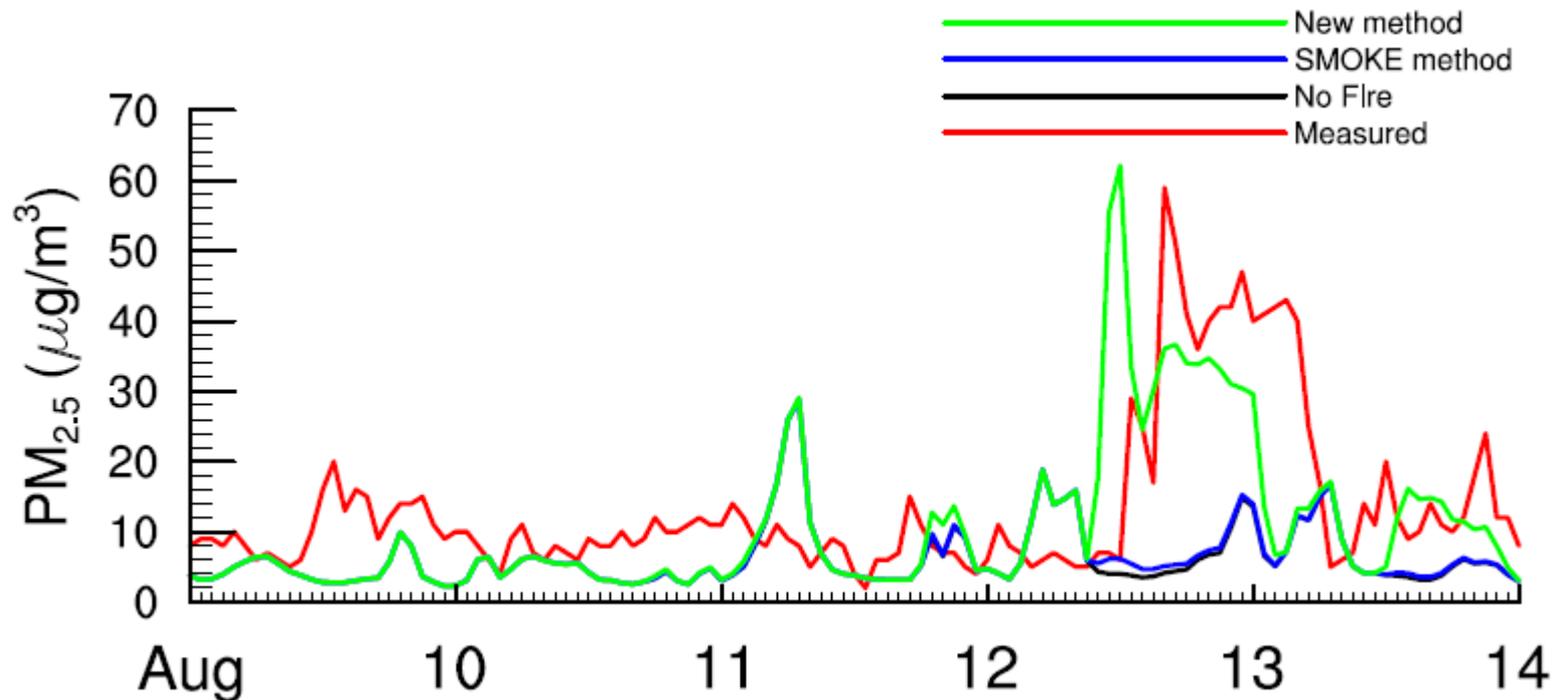
# New Method Result (3)

## Time series at St Lukes



# New Method Result (4)

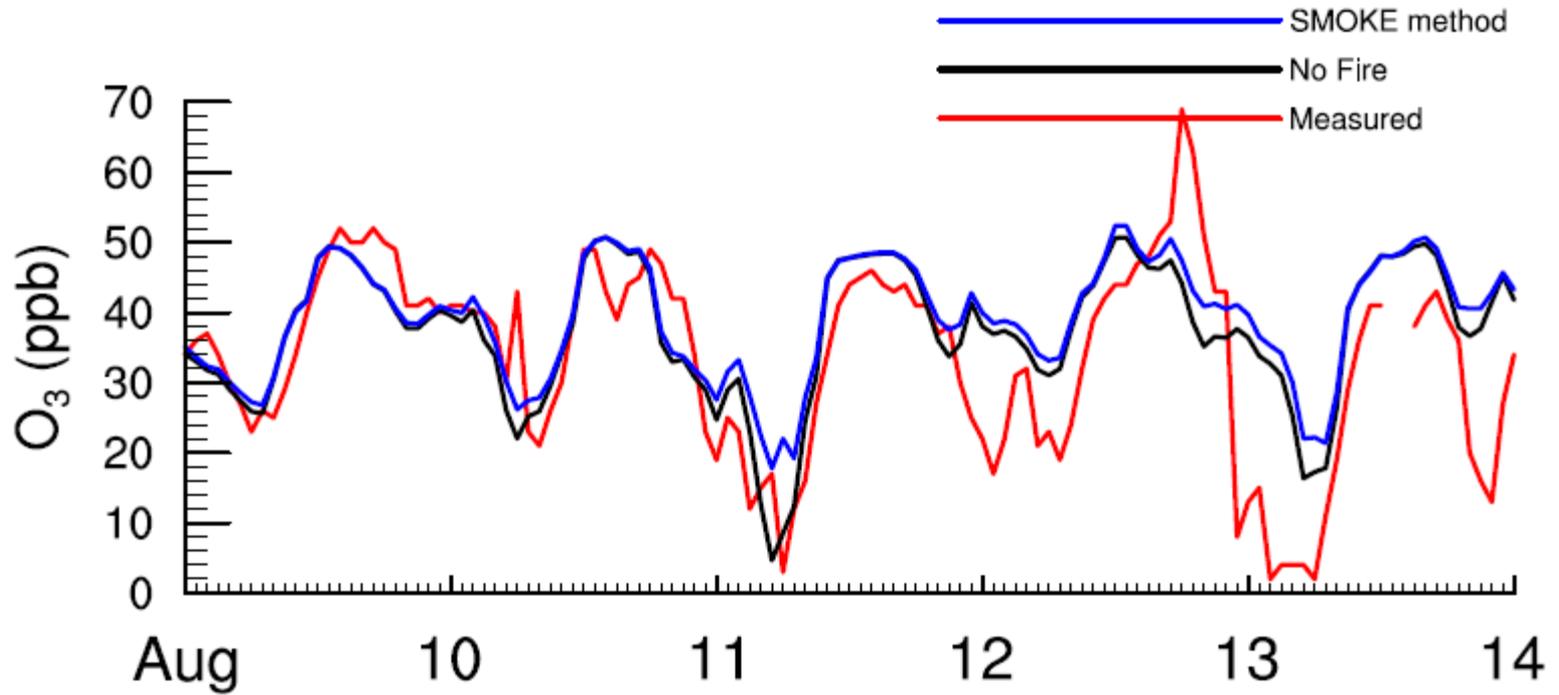
## Time series at Nampa



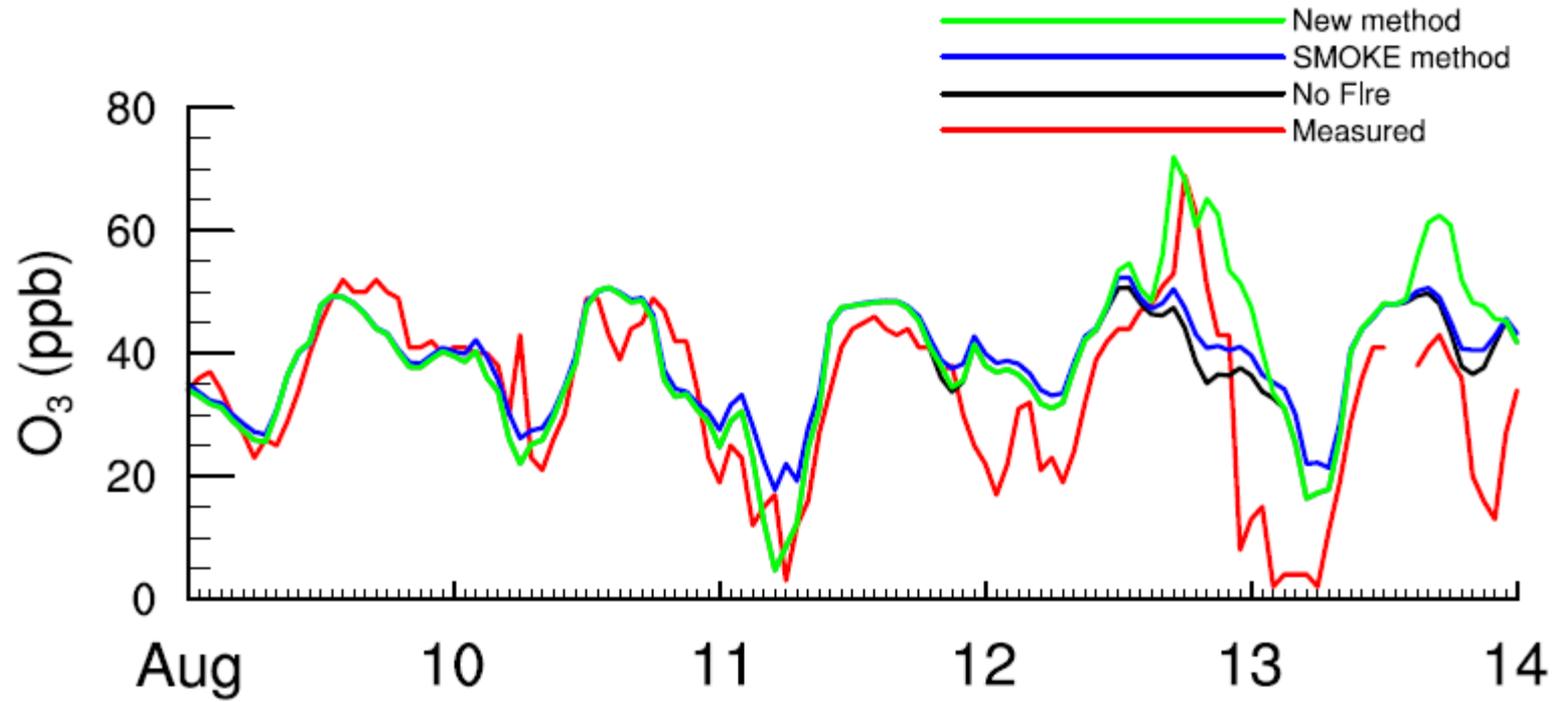
Questions???

# **SUPPLEMENTARY SLIDES**

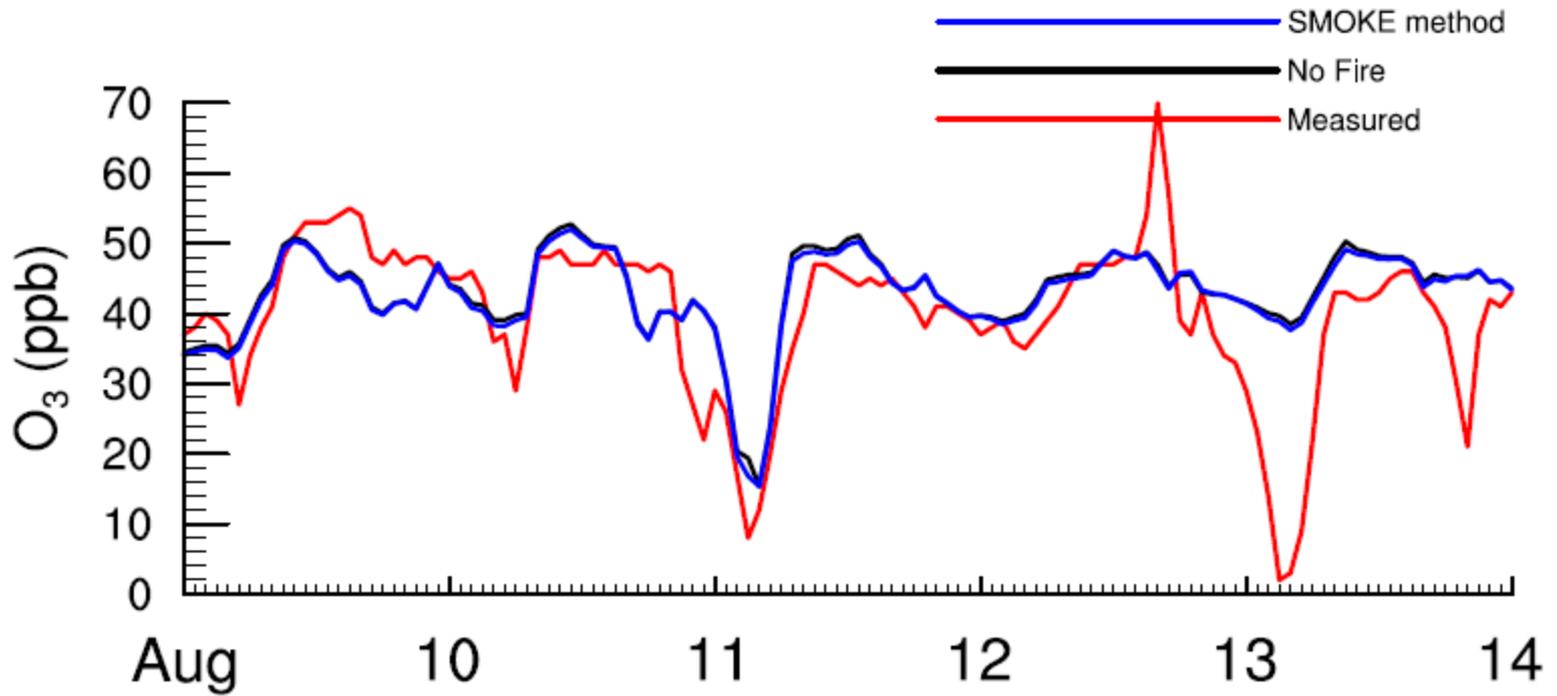
# St Lukes



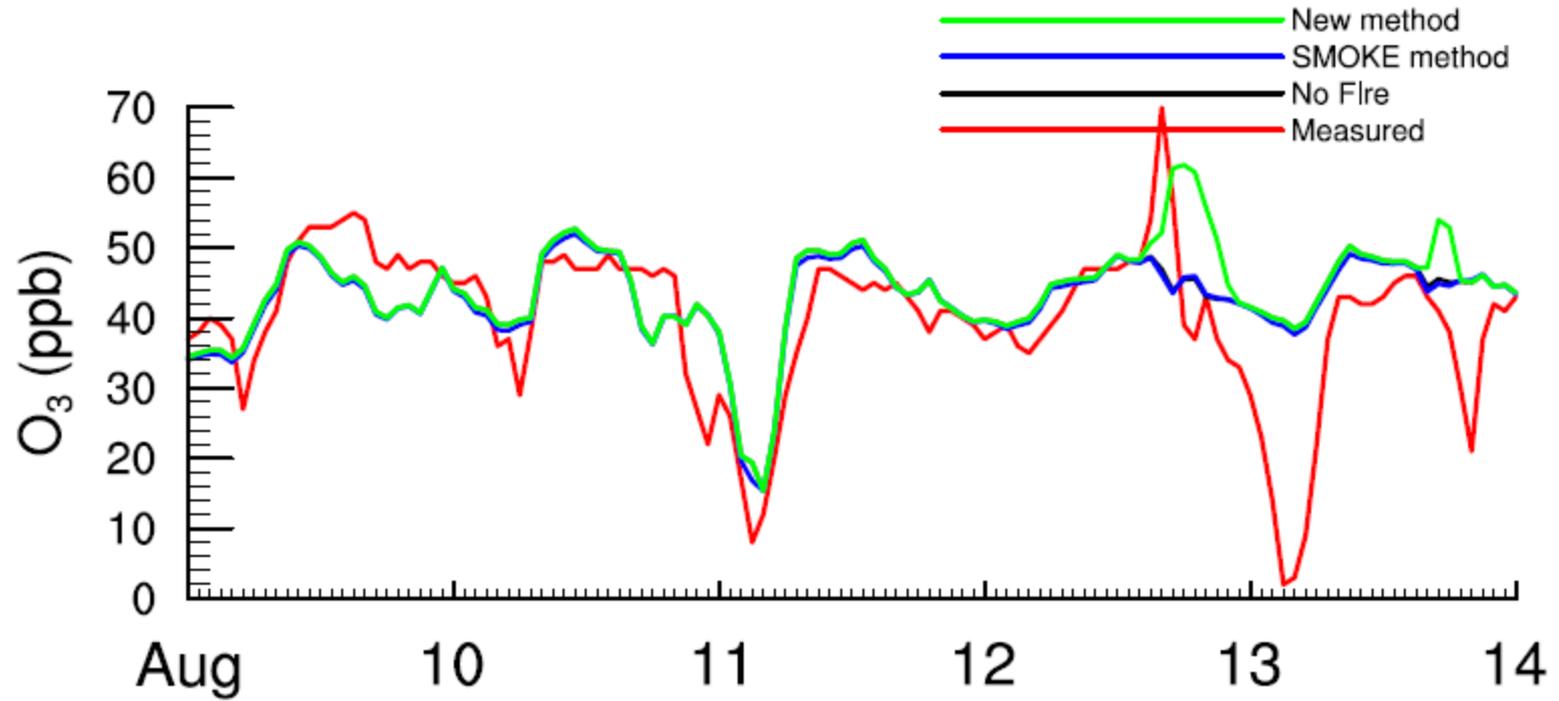
# St Lukes

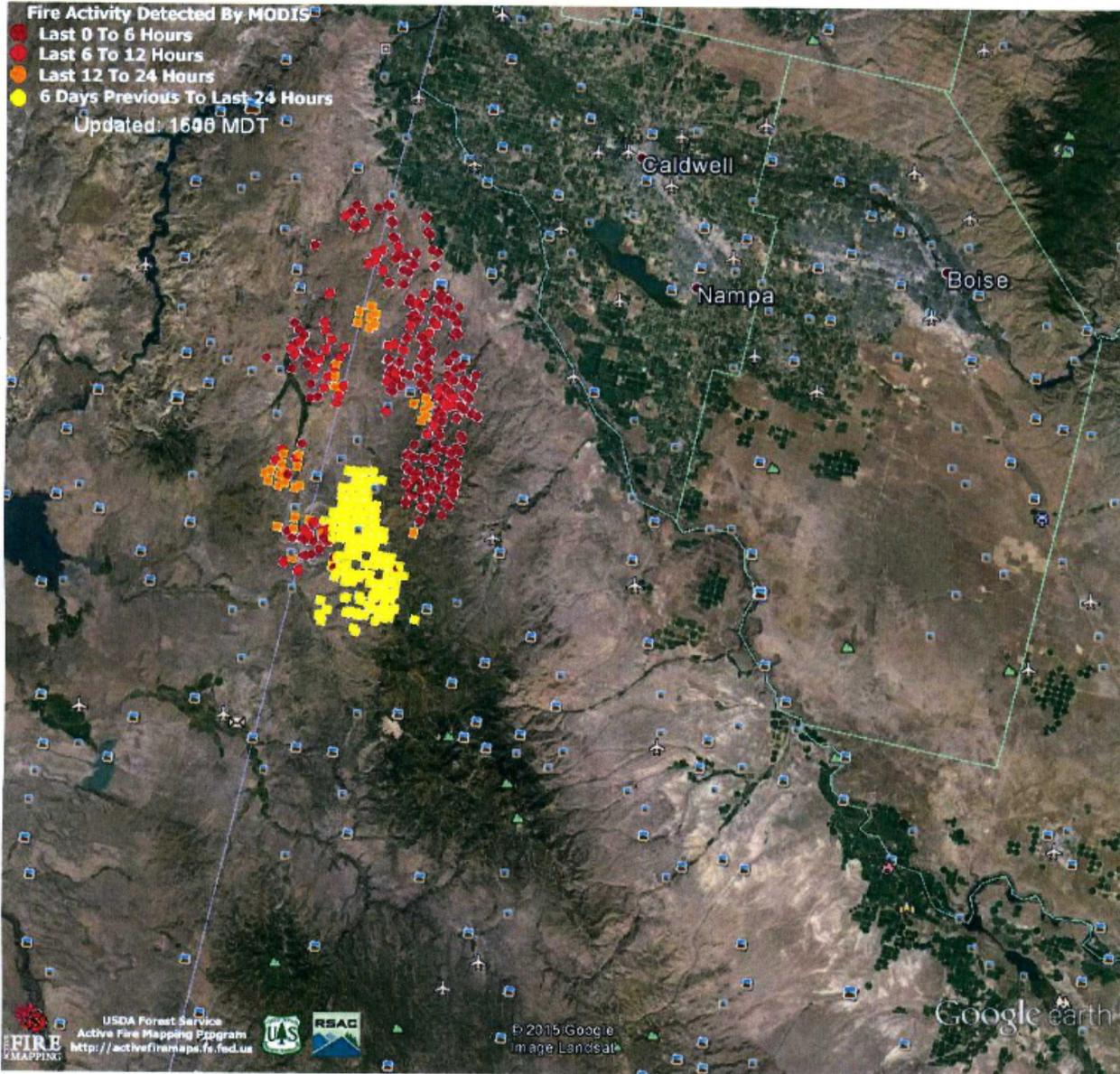


# White Pine



# White Pine





Google earth



## **Plume rise is dependent on intensity of the burn, not just total fuel consumption:**

By using the actual flaming-phase fuel consumed, the Flaming Phase Consumption Index (FPCI) looks at the *actual* heat released instead of the *potential* heat released. In addition, dividing by the square root of the acres burned attempts to capture the intensity of the burn: 1,000,000 British Thermal Units (BTUs) released over 100,000 acres is not equivalent, in terms of plume rise, to the same amount of heat released over 10,000 acres.

### **Equation 1. FPCI Calculation Used to Determine Plume Height Bins**

$$FPCI = \frac{\text{Flaming Phase Consumption}}{\sqrt{\text{acres}}}$$

### ***Lay1f Emissions Vertical Distribution***

- Lay1f fire emissions = Surface to  $\text{Max}(P_{\text{bot}}, \text{PBL})$

### ***Vertical Distribution of Elevated $P_{\text{bot}}$ to $P_{\text{top}}$ Fire Emissions (1-Lay1f)***

- 1-Lay1f fire emissions =  $P_{\text{bot}}$  to  $\text{Max}(P_{\text{top}}, \text{PBL})$

Thus, in the case where the plume bottom is greater than the PBL height ( $P_{\text{bot}} > \text{PBL}$ ), the Lay1f fire emissions are emitted from the surface to  $P_{\text{bot}}$  and the elevated (1-Lay1f) fire emissions are emitted in layers from  $P_{\text{bot}}$  to  $P_{\text{top}}$ . In the case where the PBL height is between  $P_{\text{bot}}$  and  $P_{\text{top}}$ , then both the Lay1f and the 1-Lay1f emissions are emitted in layers spanning  $P_{\text{bot}}$  and the PBL height, with the Lay1f emissions also emitted between the ground and  $P_{\text{bot}}$ . If the PBL height is above  $P_{\text{top}}$ , then the Lay1f emissions are emitted from the ground to the PBL height and the 1-Lay1f emissions are emitted between  $P_{\text{bot}}$  to the PBL height.