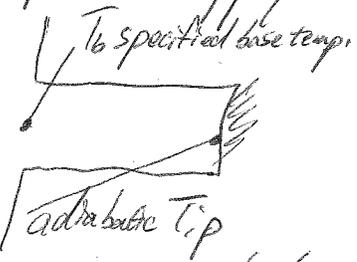


Step 7: Apply BC's (Problem Specific)



$T_b$  is easy, no interface balance required  $T_{x=0} = T_b$   
 $T = C_1 \exp(mx) + C_2 \exp(-mx) + T_\infty \Rightarrow T_b = C_1 + C_2 + T_\infty$

Interface balance @ tip:  $q_{in} = q_{out} \Rightarrow -kA_c \left( \frac{dT}{dx} \right)_{x=L} = 0 = \left( \frac{dT}{dx} \right)_{x=L}$   
 Take derivative of general solution:  $-kA_c$

$$\frac{dT}{dx} = C_1 m \exp(mx) - C_2 m \exp(-mx) = \left( \frac{dT}{dx} \right)_{x=L} = C_1 m \exp(mL) - C_2 m \exp(-mL) = 0$$

2 eqs & 2 unknowns:  $C_1 = \frac{(T_b - T_\infty) \exp(-mL)}{\exp(-mL) + \exp(mL)}$  &  $C_2 = \frac{(T_b - T_\infty) \exp(mL)}{\exp(-mL) + \exp(mL)}$

Substituting in we arrive @ the well known solution:

$$\frac{T - T_\infty}{T_b - T_\infty} = \frac{\exp(-mL(1 - \frac{x}{L})) + \exp(mL(1 - \frac{x}{L}))}{\exp(-mL) + \exp(mL)} = f(mL, \frac{x}{L})$$

Remember that  $m = \sqrt{\frac{per h}{kA_c}}$  &  $R_{cond} = \frac{L}{kA_c}$ ,  $R_{conv} = \frac{1}{hperL} \Rightarrow m = \sqrt{\frac{R_{cond}}{R_{conv}}}$

\* Show mL plot

→ There is actually a more compact way to write fin equations.

→ hyperbolic <sup>cos</sup>sine (~~sinh~~) & hyperbolic <sup>sinh</sup>sine are defined as

$$\cosh(A) = \frac{1}{2} [\exp(A) + \exp(-A)] \quad \& \quad \sinh(A) = \frac{1}{2} [\exp(A) - \exp(-A)]$$

Cosh & Sinh behave a lot like cosine & sine <sup>look familiar?</sup>  $\cos^2(A) + \sin^2(A) = 1$  |  $\cosh^2(A) - \sinh^2(A) = 1$   
 $\frac{d}{dx} [\cos(A)] = -\sin(A) \frac{dA}{dx}$  |  $\frac{d}{dx} [\cosh(A)] = \sinh(A) \frac{dA}{dx}$   
 $\frac{d}{dx} [\sin(A)] = \cos(A) \frac{dA}{dx}$  |  $\frac{d}{dx} [\sinh(A)] = \cosh(A) \frac{dA}{dx}$

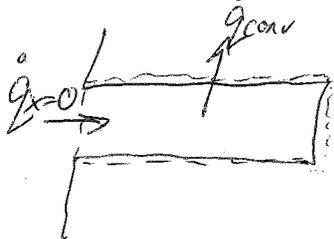
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We could've solved  $\frac{d^2 \bar{T}}{dx^2} - m^2 \bar{T} = 0$  by either  $\bar{T} = C_1 \exp(mx) + C_2 \exp(-mx)$  or

or  $\bar{T} = C_3 \sinh(mx) + C_4 \cosh(mx)$

→ this would've lead to  $\frac{\bar{T} - \bar{T}_\infty}{\bar{T}_b - \bar{T}_\infty} = \frac{\cosh[mL(1 - \frac{x}{L})]}{\cosh(mL)}$  ← much more compact & easier to write  
 write Table 1-4 pg 104

→ What about total HT from fin?



$$\dot{q}_{conv} = \int_0^L h_{per} (\bar{T} - T_\infty) dx$$

Should give same answer

$$\dot{q}_{x=0} = -kA_c \left( \frac{dT}{dx} \right)_{x=0}$$

This one likely easier as T is constant.

$$\dot{q}_{x=0} = -kA_c \frac{d}{dx} \left[ T_\infty + (T_b - T_\infty) \frac{\cosh[mL(1 - \frac{x}{L})]}{\cosh(mL)} \right]_{x=0} \Rightarrow$$

$$\Rightarrow \dot{q}_{x=0} = \frac{-kA_c (T_b - T_\infty)}{\cosh(mL)} \frac{d}{dx} (\cosh[mL(1 - \frac{x}{L})])_{x=0} \Rightarrow$$

$$\Rightarrow \dot{q}_{x=0} = \frac{-kA_c (T_b - T_\infty)}{\cosh(mL)} (-m \sinh[mL(1 - \frac{x}{L})])_{x=0} \Rightarrow$$

$$\Rightarrow \dot{q}_{x=0} = kA_c (T_b - T_\infty) \sqrt{\frac{h_{per}}{kA_c}} \tanh(mL) \leftarrow \text{same as table 1-4}$$

Also in table 1-4 is the fin efficiency:

$$\text{Fin efficiency} = \eta_{fin} = \frac{\text{fin heat transfer}}{\text{heat transfer to a "perfect" fin } (k \rightarrow \infty)}$$

(for any geometry)

$R_{cond,x} \rightarrow 0$  so the fin is isothermal at the base temp

$$\eta_{fin} = \frac{\dot{q}_{fin}}{h A_{s,fin} (T_b - T_\infty)}$$

for our rectangular fin:  $\dot{q}_{fin} = \sqrt{h \text{ per } k A_c} (T_b - T_\infty) \tanh(mL)$

$$\eta_{fin} = \frac{\sqrt{h \text{ per } k A_c} (T_b - T_\infty) \tanh(mL)}{h \text{ per } L (T_b - T_\infty)}$$

$$\eta_{fin} = \frac{\tanh(mL)}{\sqrt{\frac{h \text{ per}}{k A_c}} L} \Rightarrow \eta_{fin} = \frac{\tanh(mL)}{mL} \leftarrow \text{fin efficiency}$$

~~Show fin library in EES~~

Fin Resistance is a convenient way of accounting for fins accounts for both convection & conduction

$$\eta_{fin} = \frac{\dot{q}_{fin}}{h A_{s,fin} (T_b - T_\infty)} \Rightarrow \dot{q}_{fin} = \eta_{fin} h A_{s,fin} (T_b - T_\infty)$$

$$R_{fin} \rightarrow R_{fin} = \frac{1}{\eta_{fin} h A_{s,fin}}$$

Show fin library in EES

