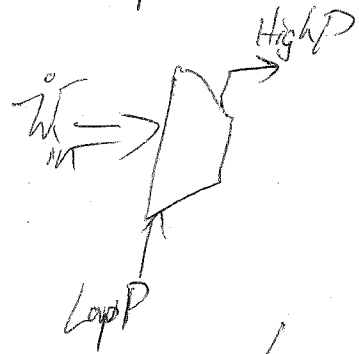


Efficiencies of Engineering Components II

Compressors: Consume power to increase the pressure of a gas
 - Reverse of a Turbine



Will an ideal compressor consume more power than a real compressor to achieve the same result? $\rightarrow$ No!!
 $\rightarrow$ The ideal does more with less

Logical definition of compressor efficiency: $\eta_{comp} = \frac{W_{ideal}}{W_{actual}}$
 W_{ideal} is the power consumed by a reversible compressor to do the same job. W_{actual} is the actual power consumed by the compressor.

Same job? 1) Same fluid/inlet conditions, 2) Same exit pressure

$\rightarrow$ To have η_{comp} be a true efficiency ≤ 1 this is the inverse of a turbine

$$\eta_{comp} = \frac{W_{ideal}}{W_{actual}} = \frac{h_2s - h_1}{h_2 - h_1} \quad \leftarrow \text{for comp that is } \begin{matrix} 1) \text{ adiabatic, } 2) \text{ P.E. \& K.E. = 0, } 3) \text{ Inlet } \\ \text{I}_{exit} \end{matrix}$$

$\rightarrow$ from here it's the same game as the turbine 4) steady state

Pumps: Similar to compressors, usually run on liquid, so it's usually/sometimes acceptable to assume incompressible substance.

If not incompressible (real fluid) then analysis is same as compressor

$$\eta_{pump} = \frac{W_{ideal}}{W_{actual}} \quad \leftarrow \text{for an incompressible substance there is a more common relationship}$$

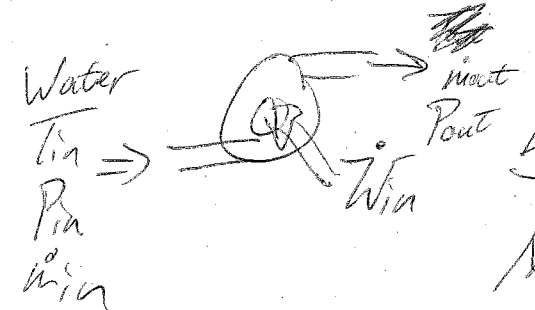
IC rules:

1) $v = \text{constant}$ 2) $u = f(T) \Rightarrow u_2 - u_1 = C(T_2 - T_1)$

3) $h = f(T) \Rightarrow h_2 - h_1 = C(T_2 - T_1) + v(P_2 - P_1)$, 4) $S_2 - S_1 = C \ln\left(\frac{T_2}{T_1}\right)$ if $S_2 = S_1$, then $T_2 = T_1$

20.2 ME301 Sp2011

Let's find the pump efficiency for an incompressible substance



Entropy Balance on Reversible pump: $\dot{S}_{in} + \dot{S}_{gen} = \dot{S}_{out} + \frac{dS_{stored}}{dt}$

$\dot{m}_{in} \dot{S}_{in} = \dot{m}_{out} \dot{S}_{out}$ $\dot{S}_{in} = \dot{S}_{out}$ $T_{2s} = T_1$ $\dot{v}_{2s} = \dot{v}_1$

Energy Balance on Reversible Pump: $\dot{E}_{in} = \dot{E}_{out} + \frac{dE_{stored}}{dt}$ $\Rightarrow 0$

$\dot{W}_{in,ideal} + \dot{m} h_1 = \dot{m} h_{2s} \Rightarrow \dot{W}_{in,ideal} = \dot{m} (h_{2s} - h_1) \Rightarrow$

$\Rightarrow \dot{W}_{in,ideal} = \dot{m} [C(T_2 - T_1) + v(P_2 - P_1)] \Rightarrow \dot{W}_{in,ideal} = \dot{m} v (P_2 - P_1)$

Actual Energy Balance on Actual Pump: $\dot{E}_{in} = \dot{E}_{out} + \frac{dE_{stored}}{dt}$

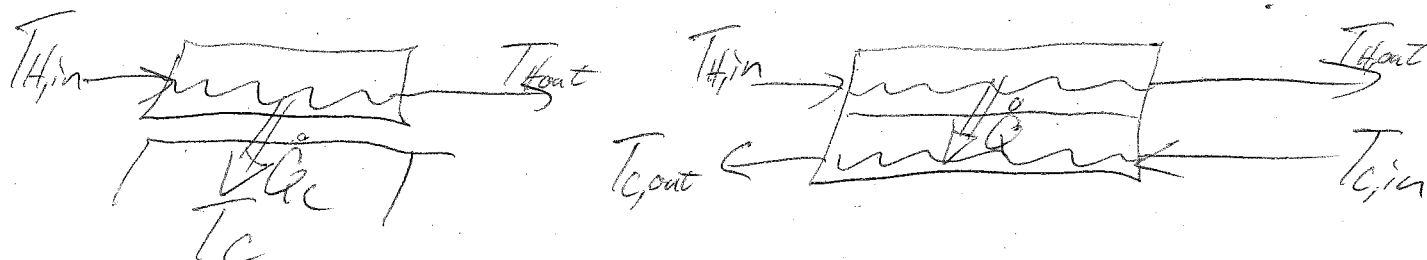
$\dot{W}_{in,actual} + \dot{m} h_1 = \dot{m} h_2 \Rightarrow \dot{W}_{in,actual} = \dot{m} (h_2 - h_1)$ $\dot{m} v = \dot{V}$

$\eta_{pump} = \frac{\dot{W}_{ideal}}{\dot{W}_{actual}} \Rightarrow \dot{W}_{actual} = \frac{\dot{W}_{ideal}}{\eta_{pump}} \Rightarrow \dot{W}_{actual} = \frac{\dot{V} \Delta P}{\eta_{pump}}$

This form is a handy result that comes up a lot (fluid mechanics)
it is handy for pumps, fans, blowers, anything with constant v
Also handy for using pump curves. I won't make you do this.

Heat exchangers; Last component we need to talk about.

↳ Transfer heat from a fluid to a ^{thermal} temperature reservoir or more often from 1 fluid to another.



Heat exchanger efficiency is ~~defined~~ called effectiveness: ϵ

ϵ is defined a little differently than other component efficiencies.

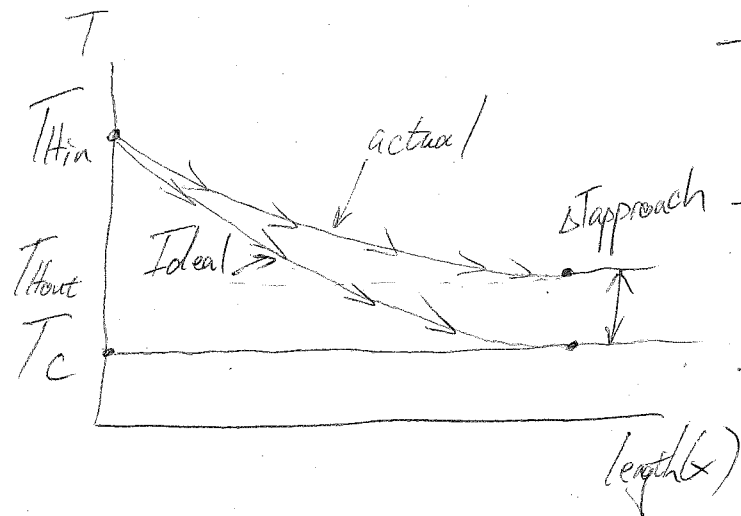
It's not defined relative to a reversible heat exchanger.

Why? → because reversible heat exchangers are not possible

$$\epsilon = \frac{\dot{Q}}{\dot{Q}_{\text{Max}}} \leftarrow \text{actual heat exchange rate in HEX}$$

$\dot{Q}_{\text{Max}} \leftarrow$ Maximum possible heat exchange rate in ideal heat exchanger
not a reversible heat exchanger

For a Cold Thermal Reservoir: Best Possible HEX brings $T_{H,\text{out}}$ down to T_C



- This defines ideal limit, $\dot{Q}_{\text{Max}}$: occurs when temperatures are the same (called the pinch point)

- The ΔT between the actual stream & the Pinch point / ideal is called the approach temperature

- The ideal HEX has a $\Delta T_{\text{approach}} = 0$

20.4 ME301 Sp2011

If I told you this heat exchanger had a $\Delta T_{\text{approach}} = 4\text{K}$

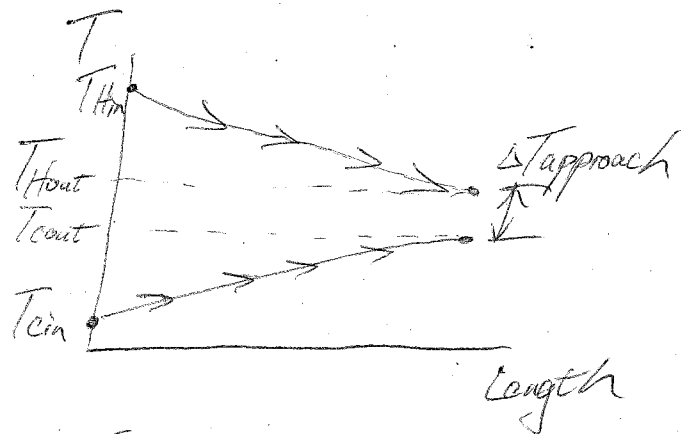
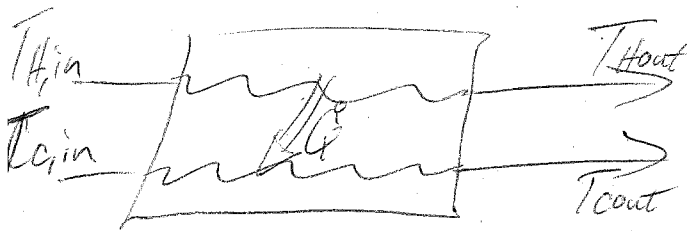
& $T_c = 300\text{K}$, what would be the outlet T , $T_{H,\text{out}} = ? = 304\text{K}$

$$\epsilon = \frac{\dot{Q}}{\dot{Q}_{\text{max}}} = \frac{\dot{M}(h_{\text{in}} - h_{\text{out}})}{\dot{M}(h_{\text{in}} - h_{\text{out,ideal}})} \quad \leftarrow \text{for cooling stream}$$

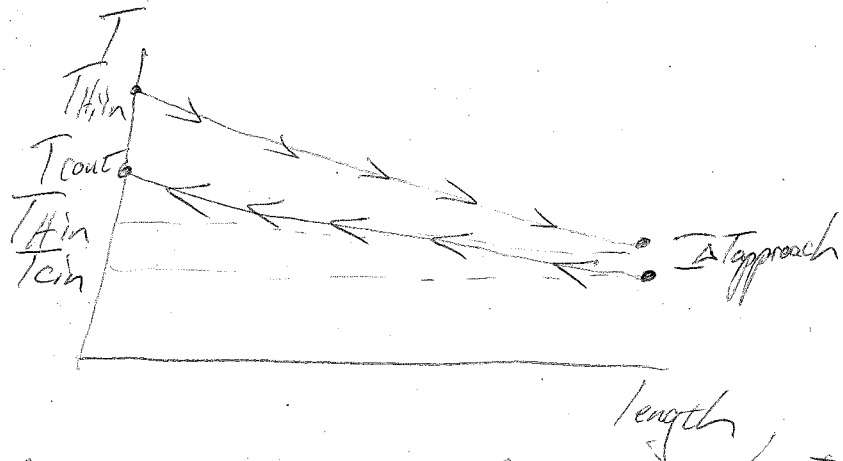
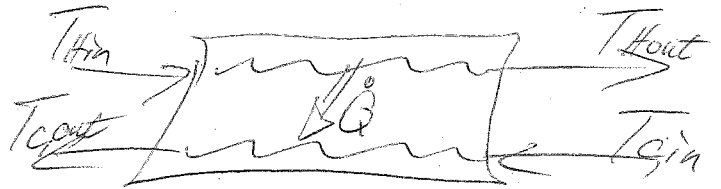
$$T_{H,\text{out,ideal}} = ? = 300\text{K} = T_c$$

Dual fluid HEX's are a little more difficult

Parallel Flow



Counter Flow



These get tough! In heat transfer you will do a lot of these & learn ^{how to} determine the location of a pinch point. In this class you will be given the location of the pinch point & either the $\Delta T_{\text{approach}}$ or ϵ .