

Jianqi Qi^{a,b}, Ying Wang^{a,b}, Xiumin Xie^{a,b}, Yuezhong Wang^{a,b}, Jicheng Zhou^a, Nian Wei^{a,b}, Jun Wang^c, Di Wu^d, Tiecheng Lu^{a,b,e}

^aSchool of Physical Science and Technology, Sichuan University, Chengdu, Sichuan, P.R. China

^bKey Laboratory of High Energy Density Physics of Ministry of Education, Sichuan University, Chengdu, Sichuan, P.R. China

^cSchool of Science, Sichuan University of Science and Engineering, Zigong, Sichuan, P.R. China

^dPeter A. Rock Thermochemistry Laboratory and NEAT ORU, University of California, Davis, USA

^eInternational Center for Material Physics, Chinese Academy of Sciences, Shenyang, Liaoning, P.R. China

Effects of Al₂O₃ phase composition on AlON powder synthesis via aluminothermic reduction and nitridation

Using micro-sized aluminum powder (11 wt.%) and nano-sized Al₂O₃ powder (89 wt.%) with five different phase compositions, AlON powders were synthesized at different temperatures in flowing-nitrogen atmosphere. Our results suggest that for starting materials with low γ -Al₂O₃/total Al₂O₃ ratio R (0 and 0.15), a calcination temperature of 1750 °C is required to obtain single-phase AlON. This temperature is about 50 °C higher than for other batches starting with larger R values (0.5, 0.85, and 1.0). The AlON powders fabricated from reactants with a high R value in this work show narrower particle size distribution and better particle homogeneity than those prepared from batches with lower R values.

Keywords: Single-phase AlON powder; Aluminothermic reduction and nitridation method; Raw materials composition; Reaction process

1. Introduction

Aluminum oxynitride spinel (γ -AlON) is a very important phase of the Al₂O₃-AlN pseudobinary solid-solution system with a composition of Al₂₃O₂₇N₅ (9Al₂O₃ · 5AlN). Due to its isotropic cubic structure, AlON can be sintered to a fully dense ceramic with high in-line transmittance and wide wavelength transmission range. Its unique mechanical and chemical properties make AlON a promising candidate for many scientific, technological, and environmental applications under extreme conditions, such as high-temperature infrared (IR) windows, illumination-saving domes, and highly transparent armors [1–3].

Despite a large number of research investigations, the application of highly transparent ceramic remains limited due to the lack of economic and feasible fabrication methods for high-quality AlON powder. Specifically, previous studies have shown that as a non-oxide ceramic material, AlON can only be synthesized by means of high-temperature solid-state reaction methods [4–8] because strong crystalline

coarsening can hardly be avoided under high synthesis temperature (above 1500 °C). Therefore, reduction and precise control of the synthesis temperature is crucial in the preparation of AlON powder.

Compared with other methods [4–8], it is easy to fabricate AlON compounds through a preminent solid-state synthesis method called aluminothermic reduction and nitridation (ARN), in which Al₂O₃ and aluminum (high-reactivity) powders are mixed as starting materials [7, 8]. However, there remain several issues to be addressed, one of which is the influence of the composition of raw starting materials. The weight ratio, phase composition, and particle size of reactants, which are acknowledged to be crucial factors in determining the phase composition and morphology of powder products [5, 6], have not been studied and reported.

In this study, we prepared AlON powder using the ARN method using micro-sized aluminum and nano-sized Al₂O₃. Powder X-ray diffraction (XRD) and scanning electron microscopy (SEM) were utilized as the main characterization techniques. The weight ratio of γ -Al₂O₃ in total Al₂O₃, R , the particle size of the starting materials, and the thermodynamic and kinetic factors that might affect the phase composition and morphology of the final powder products are discussed in detail.

2. Experimental

Industrial-standard micro-sized aluminum powder (particle size, 1 ~ 2 μ m; purity, 99+%; Yuanyang Aluminum Industry Co., Ltd, Henan, P.R. China) and nano-sized α - and γ -Al₂O₃ powders (average crystal size for α and γ -Al₂O₃, 80 nm and 20 nm, respectively; purity, 99.99+%; Luming Nanomaterials Co., Ltd, Liaoning, P.R. China) were used as starting materials. These were ball milled to a certain weight ratio (11 wt.% for aluminum and 89 wt.% for Al₂O₃) and R value (see Table 1) in a 500 ml polyurethane jar with ZrO₂ balls (diameter, 5 mm) for 24 h in nitrogen atmosphere. Subsequently, the well-mixed powders were placed in a high-pur-

Table 1. Phase compositions of as-made AION powders calcined at various temperatures with different R values.

	$R = 0$	$R = 0.15$	$R = 0.50$	$R = 0.85$	$R = 1.0$
1650 °C	AION + Al_2O_3 + AlN	AION + Al_2O_3 + AlN	AION + Al_2O_3	AION + Al_2O_3	AION + Al_2O_3
1700 °C	AION + Al_2O_3	AION + Al_2O_3	AION	AION	AION
1750 °C	AION	AION	AION	AION	AION

ity corundum crucible, transferred into a graphite furnace (Model ZT-40-20Y; Shanghai Chenxin Electric Furnace Co., Ltd, Shanghai, P.R. China), and heated to pre-programmed temperatures (1650 °C, 1700 °C, and 1750 °C) for 3 h of ARN reaction in nitrogen flow. Finally, the final calcined products were ground, passed through a 250-mesh sieve, and ball milled for another 24 h under the same conditions as the raw material preparation.

Phase identification of the samples was carried out by means of XRD with a DX-2500 diffractometer (Dandong Fangyuan Instrument Co., Ltd, Liaoning, P.R. China). SEM was used to reveal the morphology of the final powder

products. The grain size distribution for each sample was calculated by averaging the data obtained from the SEM images.

3. Results and discussion

Figure 1 presents the XRD patterns of the powders prepared under different conditions (R value and calcination temperature). Table 1 shows the phase compositions of the products. For all products, AION was the dominative phase. Specifically, after calcination at 1650 °C, both Al_2O_3 and AlN were still present in reactants with low R values (0 and 0.15), whereas those with high R values (0.5, 0.75, and 1.0) showed Al_2O_3 as the only impurity. Heating at 1700 °C eliminated AlN from the products; however, Al_2O_3 remained in samples with low R values. At about

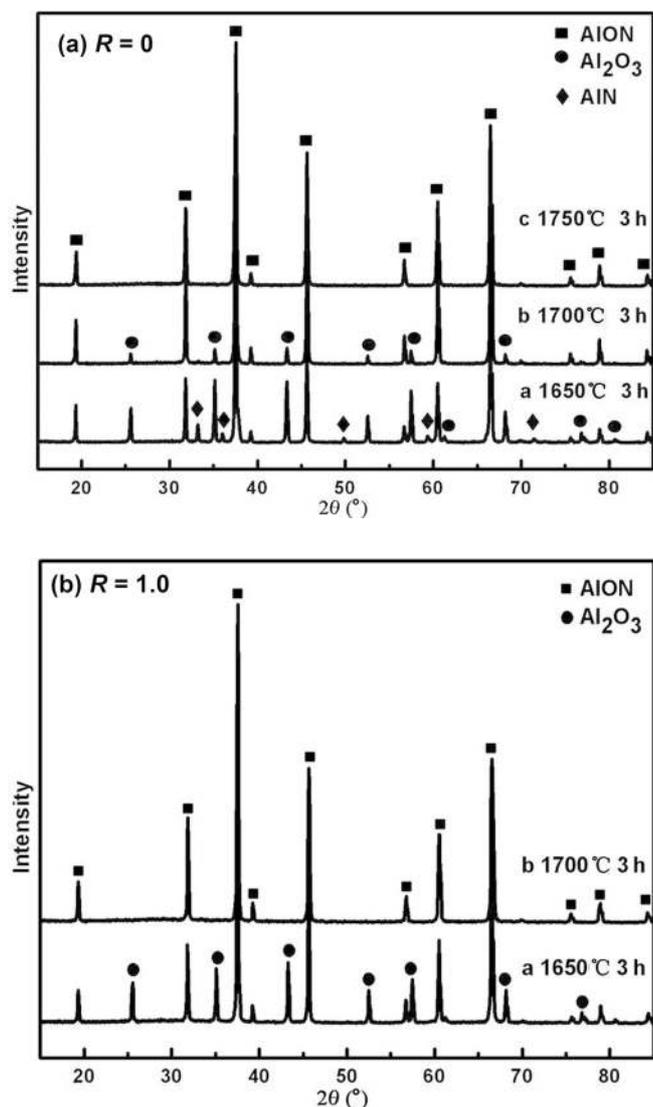


Fig. 1. Powder X-ray diffraction patterns of powder product calcined at various temperatures with different R values.

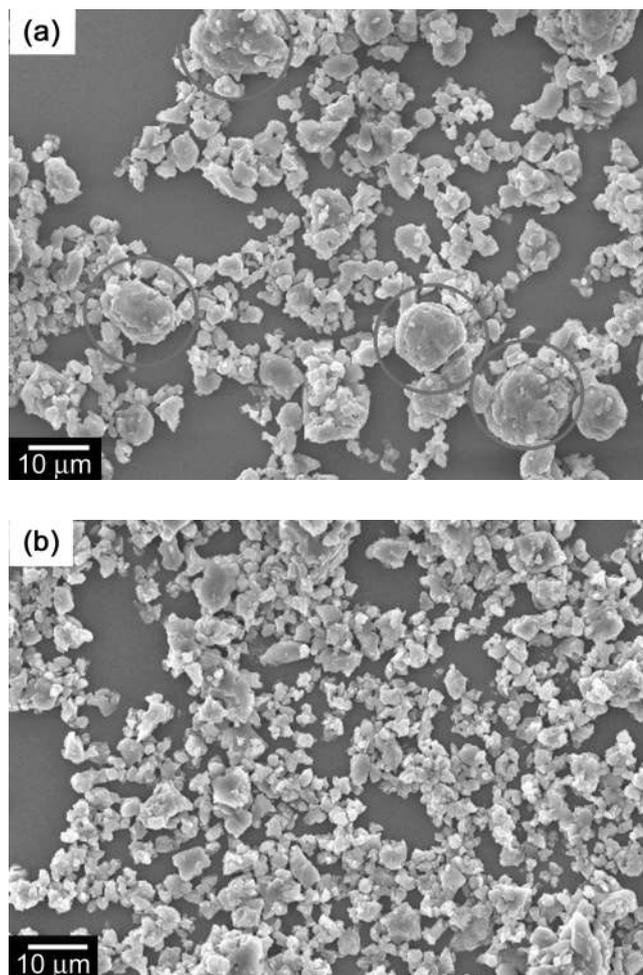


Fig. 2. SEM images of single-phase AION powder with different R values after ball milling for 24 h. (a) $R = 0$, (b) $R = 1.0$.

1750 °C, when all secondary phases had disappeared (see Fig. 1), the starting materials completely transformed into single-phase AlON. The above observations suggest that the synthesis temperature of single-phase AlON reported by us is significantly lower than that mentioned in previous studies [4, 5].

The morphology (see Fig. 2) and grain size distribution profiles (see Fig. 3) suggest that for all the powder products, the grain sizes fall within the range of 1 to 10 micrometers. Interestingly, powders calcined at lower temperatures have smaller particle sizes and preserve better particle uniformity. Additionally, the product particle distribution tends to be narrower and closer to its Gaussian distribution as the *R* value increases. Thus, our synthesis fabricated materials with better quality than that of samples prepared by means of other solid-state synthesis methods [4, 9]. Our method may further benefit the sintering of highly transparent ceramics [10]. Also, the experimental observations from reduced-temperature synthesis of single-phase AlON powder strongly suggest that our method has the advantages of reducing the agglomeration of the final AlON product powder and lowering production cost [4, 5, 9].

Due to the high reactivity of aluminum, the reaction between aluminum and Al₂O₃ usually selects a self-propagating high-temperature synthesis (SHS) pathway [8]; vapor-liquid and/or vapor-liquid-solid and two-step mechanisms were suggested during the materials formation process [8]. However, the high reactivity and the short, intensive reaction period of SHS usually lead to impurity phases and a coarsened AlON sample. A large body of research has been carried out to obtain single-phase and non-coarsened AlON. Miao et al. [7] found that the SHS reaction could be

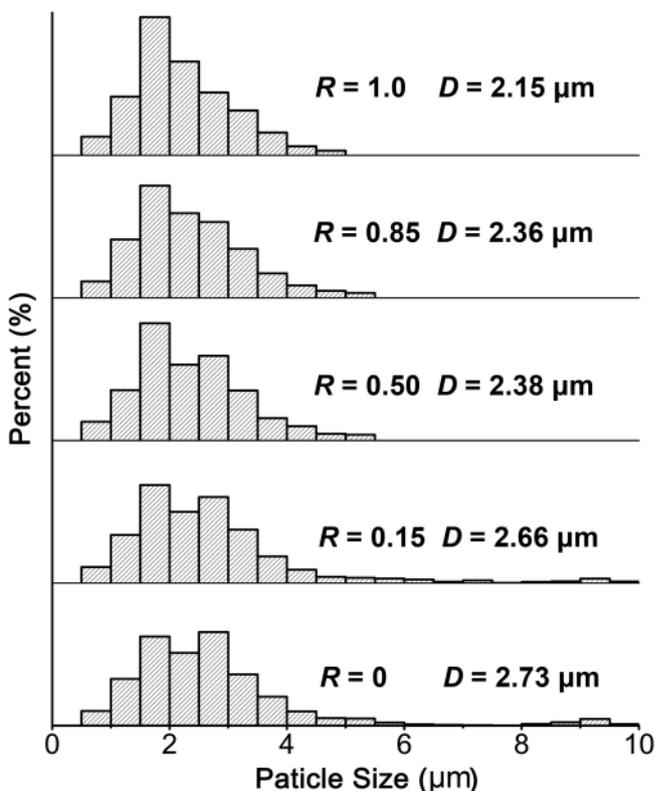


Fig. 3. Grain size distribution profiles of single-phase AlON powder.

minimized by using a small amount of aluminum as starting material. In a later report, Wang et al. [11] did a thermodynamic analysis on the ARN method. Combining the conclusions from these two earlier studies and the interpretation of our current data, a schematic of the ARN reaction process is proposed, as shown in Fig. 4, which clearly suggests that the reaction may have two consecutive steps. First, after ball milling, the reactants are uniformly mixed and the large micron-sized aluminum particles are surrounded by small nano-sized Al₂O₃ particles. The melting and nitridation reactions to produce AlN start at about the melting point of aluminum, because a well-resolved X-ray diffraction peak of AlN can be observed once the reactants are calcined at 800 °C [11]. Al₂O₃ particles are segregated into aluminum particles and then to AlN with small particle sizes through gas-solid and/or gas-liquid-solid mechanisms. All the nitridation processes are completed at about 1100 °C. Subsequently, the solid-state reaction between AlN and Al₂O₃ is initiated at about 1600 °C, which is defined as the critical temperature for phase stabilization of AlON, providing enough thermodynamic driving force for the reaction. As the AlON-stabilized region expands with increasing temperature [11, 12], the formation of AlON accelerates accordingly. Therefore, our reaction at 1700 °C with 3 h of isothermal calcination is more than enough for the formation of single-phase AlON with high *R* values.

The phase composition of Al₂O₃ reactant powder is also a crucial factor affecting the thermodynamic states and kinetic reaction pathways. The nano-Al₂O₃ powders used in this work provide an additional driving force because of their large surface area and high-energy disordered surfaces. McHale et al. [13, 14] reported that for γ - and α -Al₂O₃ nanoparticles with the same size, γ -Al₂O₃ is a thermodynamically preferable phase. In other words, α -Al₂O₃ is less stable on the nanoscale. This phenomenon also explains why nano-Al₂O₃ is more common in the γ phase. Interestingly, McHale et al. also suggested that coarsening of γ -Al₂O₃ happens at about 900 °C for γ -Al₂O₃ (166 m² g⁻¹) and at 500 °C (156 m² g⁻¹) for α -Al₂O₃. In our current work, γ -Al₂O₃ with an average particle size of 20 nm was used instead of α -Al₂O₃ (80 nm). The strong resistance to coarsening maintains a high surface area for γ -Al₂O₃ under high

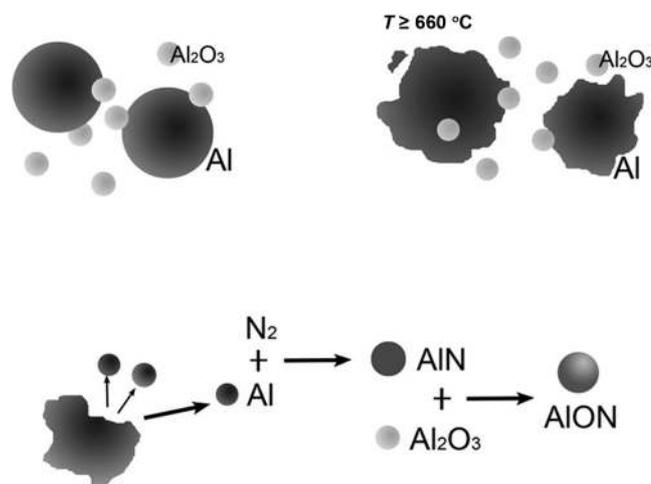


Fig. 4. Schematic of reaction process based on ARN (aluminothermic reduction and nitridation) method.

temperature, which enables the surface energy contribution during nitridation of aluminum. Additionally, although the solid-state reaction process is usually governed by the diffusion of solid materials, the γ -Al₂O₃ nanoparticles used in this work offer an effective free path necessary for transport, especially ion diffusion. Hence, compared with the conventional methods, the higher ratio of γ -Al₂O₃ used in this work can provide both a stronger thermodynamic driving force at the start of the reaction as well as better diffusion in later reaction processes. Moreover, the coarsening prohibition of γ -Al₂O₃ can avoid the formation of big AlON grains during the reaction process, as shown in the grain size distribution of single-phase AlON powders (see Figs. 2 and 3), in which big particles occur only with a low *R* value.

This work was supported by the National Science Foundation of P.R. China (Grant Nos. 51002098 and 91326103), the Fund of Aeronautics Science (Grant No. 20100119003), and the Talent Introduction Programme of Sichuan University of Science and Engineering (Grant No. 2013RC07). All analyses were done at the Analytical and Testing Center of Sichuan University.

References

- [1] J.W. McCauley: *J. Am. Ceram. Soc.* 61 (1978) 372. DOI:10.1111/j.1151-2916.1978.tb09336.x
- [2] N.D. Corbin: *J. Eur. Ceram. Soc.* 5 (1989) 143. DOI:10.1016/0955-2219(89)90030-7
- [3] J.W. McCauley, P. Patel, M.W. Chen, G. Glide, E. Strassburger, B. Paliwal, K.T. Ramesh, D.P. Dandekar: *J. Eur. Ceram. Soc.* 29 (2008) 223. DOI:10.1016/j.jeurceramsoc.2008.03.046
- [4] S. Bandyopadhyay, G. Rixecker, F. Aldinger, S. Pal, K. Mukherjee, H.S. Maiti: *J. Am. Ceram. Soc.* 85 (2002) 1010–1012. DOI:10.1111/j.1151-2916.2002.tb00212.x
- [5] Y.W. Li, N. Li, R.Z. Yuan: *J. Mater. Sci.* 34 (1999) 2547. DOI:10.1023/A:1004477910514
- [6] J. Zheng, B. Forslund: *J. Eur. Ceram. Soc.* 15 (1995) 1087. DOI:10.1016/0955-2219(95)00078-9
- [7] W.F. Miao: US Patent (2005) 695579.
- [8] D. Zientara, M.M. Bucko, J. Lis: *J. Eur. Ceram. Soc.* 27 (2007) 775–779. DOI:10.1016/j.jeurceramsoc.2006.04.008
- [9] R. Bachelard, J. Disson, B. Morlhon: US Patent (1997) 5688730.
- [10] Y.Z. Wang: Ph.D. Thesis, Sichuan University, Chengdu, China (2012).

- [11] Y.Z. Wang, T.C. Lu, Y. Yu, J.Q. Qi, J.S. Wen, H.P. Wang, L. Xiao, Z.L. Yang, J. Yu, Y. Wen, N. Wei: *Rare Metal Mat. Eng.* 38 (2009) S48.
- [12] H.X. Willems, M.M.R.M. Hendrix, R. Metselaar, G. De With: *J. Eur. Ceram. Soc.* 10 (1992) 327. DOI:10.1016/0955-2219(92)90088-U
- [13] J.M. McHale, A. Auroux, A.J. Perrotta, A. Navrotsky: *Science* 277 (1997) 778. DOI:10.1126/science.277.5327.788
- [14] J.M. McHale, A. Navrotsky, A.J. Perrotta: *J. Phys. Chem. B* 101 (1997) 603. DOI:10.1021/jp9627584

(Received June 4, 2013; accepted November 21, 2013)

Bibliography

DOI 10.3139/146.111032
 Int. J. Mater. Res. (formerly Z. Metallkd.)
 105 (2014) E; page 1–4
 © Carl Hanser Verlag GmbH & Co. KG
 ISSN 1862-5282

Correspondence address

Prof. Jianqi Qi, or Prof. Tiecheng Lu
 Department of Physics
 Sichuan University
 29 Wangjiang Road
 Wuhou District
 Chengdu, 610064
 P. R. China
 Tel: +86-028-85412322
 Fax: +86-028-85412322
 E-mail: qijianqi@scu.edu.cn, lutiecheng@scu.edu.cn

You will find the article and additional material by entering the document number **MK111032** on our website at www.ijmr.de